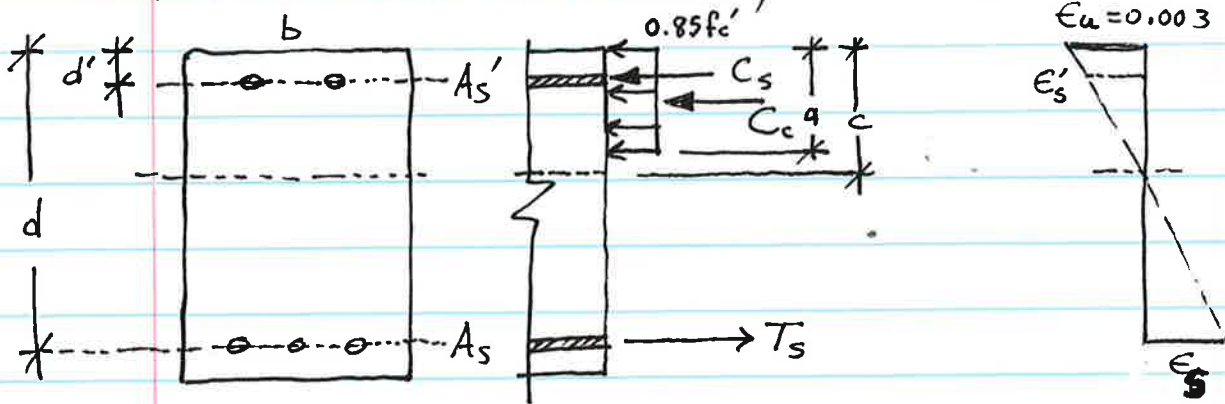


①

Rectangular Beams With Compression Reinforcement. "Doubly" Reinforced Beams



- By horizontal Equilibrium (assuming A_s' is above c)

$$T_s = C_s + C_c \quad (1)$$

$$\Rightarrow A_s f_y = \underbrace{A_s' (f_s' - 0.85 f_c')}_{C_s} + \underbrace{0.85 f_c' b a}_{C_c} \quad (2)$$

where $f_s' = E_s \epsilon_s'$ (3)

- Strain Compatibility requires that

$$\frac{\epsilon_s}{d-c} = \frac{\epsilon_u}{c} \Rightarrow \epsilon_s = \epsilon_t = \left(\frac{d-c}{c}\right) \epsilon_u \quad (4)$$

and

$$\frac{\epsilon_s'}{c-d'} = \frac{\epsilon_u}{c} \Rightarrow \epsilon_s' = \left(\frac{c-d'}{c}\right) \epsilon_u \quad (5)$$

- Nominal Moment Capacity (once c is known)

$$M_n = C_c \left(d - \frac{a}{2}\right) + C_s (d - d') \quad (6)$$

- Determine ϕ based on ϵ_t
- Check f_{min} and $\epsilon_t > 0.004$ which is max. requirement.

• Case of compression steel yielded.

$$\rightarrow f_s' = f_y$$

$$\text{-From (2)} \Rightarrow a = \frac{A_s f_y - A_s' (f_s' - 0.85 f_c')}{0.85 f_c' b}$$

-From (6)

(by summing moments about tensile steel)

$$M_n = 0.85 f_c' b a \left(d - \frac{a}{2} \right) + A_s' (f_y - 0.85 f_c') (d - d')$$

-Calculate ϕ based on ϵ_t

-Check f_{min} and max limitation of $\epsilon_t > 0.004$

$$f_{min} = \frac{200}{f_y} \quad \text{or} \quad \frac{3\sqrt{f_c'}}{f_y} \quad (\text{the greater of these is } f_{min})$$

(3)

- Case of Compression Steel Not Yielded

- From (2) $\Rightarrow A_s f_y = A_s' (f_s' - 0.85 f_c') + 0.85 f_c' b a$

- Using (3) and (5) $T = C_s + C_c$

$\Rightarrow A_s f_y = A_s' \left(E_s \left(\frac{c-d'}{c} \right) \epsilon_u - 0.85 f_c' \right) + 0.85 f_c' b \beta_1 c$ (*)

- Solve equation (*) for c by trial and error.
see text p. 144 W&M 5th

- Once c is found calculate $a = \beta_1 c$

- Calculate $f_s' = E_s \left(\frac{c-d'}{c} \right) \epsilon_u$

- Calculate M_n (by summing moments about tensile steel)

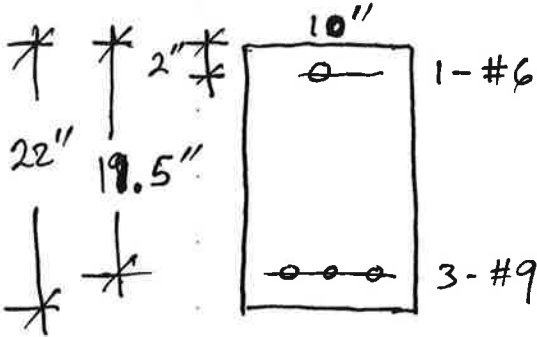
$$M_n = 0.85 f_c' b a \left(d - \frac{a}{2} \right) + A_s' (f_s' - 0.85 f_c') (d - d')$$

- Calculate ϕ based on $\epsilon_t = \left(\frac{d-c}{c} \right) \epsilon_u$

- Check f_{min} and max. requirement of $\epsilon_t > 0.004$

Assuming.

Example - case of Compression steel yielding



$f'_c = 3 \text{ ksi}$
 $f_y = 60 \text{ ksi}$

Results from computer program

$c = 7.14$

$\epsilon_t = 0.0052$ (For Verification)

$\phi = 0.9$

$M_n = 2990 \text{ k-in}$

$\phi M_n = 2691 \text{ k-in}$

Find ϕM_n

Solution: • $A_s' = 0.44 \text{ in}^2$ $A_s = 3(1) = 3 \text{ in}^2$

• We assume compression steel has yielded (tensile steel too!)

\Rightarrow from eq. (2) $\Rightarrow A_s f_y = A_s' (f_y - 0.85 f'_c) + 0.85 f'_c b a$

• Solve for a

$\rightarrow a = \frac{A_s f_y - A_s' (f_y - 0.85 f'_c)}{0.85 f'_c b} = \frac{3(60) - 0.44(60 - 0.85(3))}{0.85(3)(10)} = 6.07 \text{ in}$

• Find c

$c = \frac{a}{\beta_1} = \frac{6.07}{0.85} = 7.14 \text{ in}$

• Verify compression steel yielded

from (5) $\rightarrow \epsilon_s' = \left(\frac{c-d'}{c}\right) \epsilon_u = \frac{7.14-2}{7.14} (0.003) = 0.00216 > \epsilon_y = \frac{f_y}{E_s} = \frac{60}{29000} = 0.00207$
OK

• Calculate M_n

from (4) $\rightarrow M_n = 0.85 f'_c b a \left(d - \frac{a}{2}\right) + A_s' (f_y - 0.85 f'_c) (d - d')$
 $= 0.85(3)(10)(6.07)(19.5 - \frac{6.07}{2}) + 0.44(60 - 0.85(3))(19.5 - 2) = 2990 \text{ k-in}$

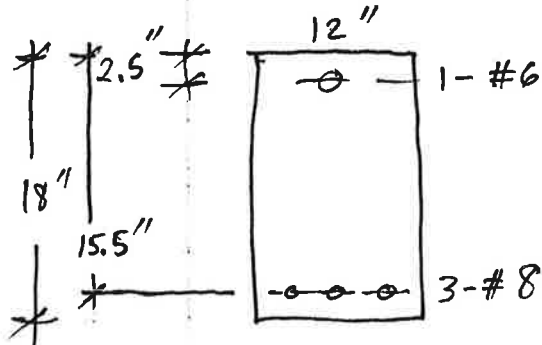
• Calculate ϵ_t

from (4) $\rightarrow \epsilon_t = \left(\frac{d-c}{c}\right) \epsilon_u = \left(\frac{19.5-7.14}{7.14}\right) 0.003 = 0.00519 > 0.005 \Rightarrow \phi = 0.9$

• Check $f_{min} = \frac{200}{f_y} = \frac{200}{60000} = 0.00333$ Max limit satisfied $\epsilon_t > 0.004$
 $\frac{3\sqrt{f'_c}}{f_y} = 0.0027$ provided $f = \frac{A_s}{b d} > f_{min}$ OK

• Calc. ϕM_n $\phi M_n = 0.9(2990) = \boxed{2691 \text{ k-in}}$

Example Case of ^{Compression} Steel Not Yielded



$f'_c = 3 \text{ ksi}$
 $f_y = 60 \text{ ksi}$

Results from Computer program

$c = 4.8 \text{ in}$
 $\epsilon_t = 0.00688$
 $\phi = 0.9$
 $M_n = 1906 \text{ k-in}$
 $\phi M_n = 1715 \text{ k-in}$
 $\epsilon'_s = 0.00144$

for Verification

Find ϕM_n

Solution: • $A'_s = 0.44 \text{ in}^2$, $A_s = 3(0.79) = 2.37 \text{ in}^2$

• If we didn't know the steel yielded, which generally is the case we proceed by guessing a value of c . See W. & M. 5th p. 144 for procedure.

• Authors suggest guess for c of between $d/4$ and $d/3$
 \Rightarrow try $c = \frac{d}{3} = \frac{15.5}{3} = 5.17 \text{ in}$

• Calc. $\epsilon'_s = \left(\frac{c-d'}{c}\right)\epsilon_u = \left(\frac{5.17-2.5}{5.17}\right)0.003 = -0.00155 < \epsilon_y$

• Check horizontal Equilibrium

$\Rightarrow T = A_s f_y = 2.37(60) = 142.2 \text{ kips}$

use positive value of strain
↓

$C_s + C_c = A'_s (E_s \epsilon'_s - 0.85 f'_c) + 0.85 f'_c b \beta_1 c = 0.44(29000(0.00155) - 0.85(3)) + 0.85(3)(12)(0.85)(5.17)$
 $= 153.1 \text{ kips}$

difference between T and $(C_s + C_c) > 5\%$

since $T < C_s + C_c$ we need to decrease c

• New guess try $c = 4.8 \text{ in}$ (← cheating since I know computer results)

• Calc. $\epsilon'_s = \left(\frac{4.8-2.5}{4.8}\right)0.003 = -0.00144 < \epsilon_y$

• Check Horizontal Equilibrium

$T = 142.2 \text{ kips}$

$C_s + C_c = 0.44(29000(0.00144) - 0.85(3)) + 0.85(3)(12)(0.85)(4.8) = 142.1 \text{ kips}$

$\Rightarrow T \approx C_s + C_c$ good! $c = 4.8 \text{ in}$ is right. →

(6)

- Check ϵ_t , to get ϕ

$$\epsilon_t = \left(\frac{d-c}{c}\right) \epsilon_u = \frac{15.5-4.8}{4.8} (0.003) = 0.00688 > 0.005$$

$$\Rightarrow \phi = 0.9$$

- Calculate Nominal Moment by summing moments about tension steel.

$$Eq(6) \rightarrow M_n = 0.85 f'_c b \beta_1 c \left(d - \frac{\beta_1 c}{2} \right) + A'_s E_s \epsilon'_s \left(f'_c d - d' \right)$$

$$= 1905 \text{ k-in}$$

- Calculate ϕM_n

$$\phi M_n = 0.9(1905) = \boxed{1714 \text{ k-in}}$$

- Check f_{min}

$$f_{min} = \frac{200}{f_y} = 0.0033 \text{ or } \frac{3\sqrt{3000}}{60000} = 0.00274 \Rightarrow f_{min} = 0.0033 \text{ governs}$$

$$f_{provided} = \frac{A_s}{bd} = \frac{2.37}{12(15.5)} = 0.0127 > f_{min} \text{ OK!}$$

- Check max. reinf. limits

$$\epsilon_t > 0.004 \therefore \text{satisfied!}$$