

Applications of Eigenvalues & Eigenvectors

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For Linear Algebra Class
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- 4 Critical loads and buckled shapes in buckling analysis
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1. The eigenvalue/eigenvector problem

Find vector \mathbf{v} and scalar λ that satisfies the following:

$$\mathbf{K}\mathbf{v} = \lambda\mathbf{v} \quad (1)$$

where,

\mathbf{K} = $n \times n$ matrix

\mathbf{v} = $n \times 1$ vector, an eigenvector

λ = a scalar, an eigenvalue

n vector and scalar pairs will satisfy equation (1). How to find such pairs is a linear algebra problem.

Equation (1) arises on occasion during the solution of various types of engineering problems

1. The eigenvalue/eigenvector problem

An example (3x3 matrix \Rightarrow 3 eigenvalues and 3 eigenvectors):

$$\begin{bmatrix} \tau_{xx} & \tau_{xy} & \tau_{xz} \\ \tau_{xy} & \tau_{yy} & \tau_{yz} \\ \tau_{xz} & \tau_{yz} & \tau_{zz} \end{bmatrix} \begin{bmatrix} v_1 \\ v_2 \\ v_3 \end{bmatrix} = \tau \begin{bmatrix} v_1 \\ v_2 \\ v_3 \end{bmatrix} \quad (2)$$

$$\begin{bmatrix} 10 & 8 & 0 \\ 8 & 14 & 5 \\ 0 & 5 & 9 \end{bmatrix} \begin{bmatrix} v_1 \\ v_2 \\ v_3 \end{bmatrix} = \tau \begin{bmatrix} v_1 \\ v_2 \\ v_3 \end{bmatrix} \quad (3)$$

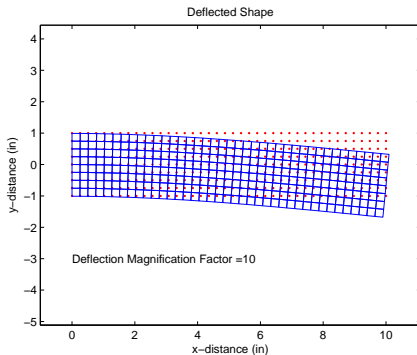
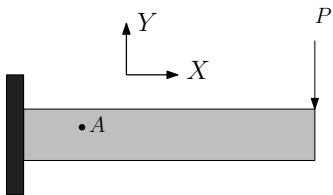
MATLAB solution to eigenvalue problem:

$$\tau_1 = 2.17, \mathbf{v} = \begin{bmatrix} -0.64 \\ 0.62 \\ -0.46 \end{bmatrix}, \quad \tau_2 = 9.29, \mathbf{v} = \begin{bmatrix} 0.55 \\ -0.05 \\ -0.83 \end{bmatrix}, \quad (4)$$

$$\tau_3 = 21.54, \mathbf{v} = \begin{bmatrix} -0.54 \\ -0.78 \\ -0.31 \end{bmatrix}$$

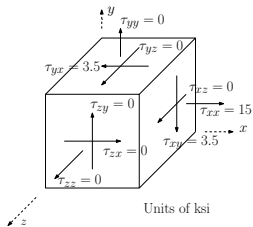
2. Principal stresses and directions in stress analysis

Consider a two dimension problem. A cantilever beam loaded at its free end.



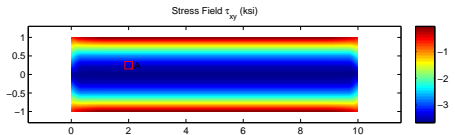
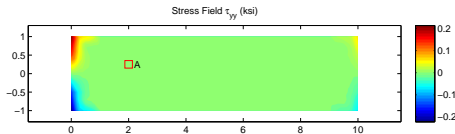
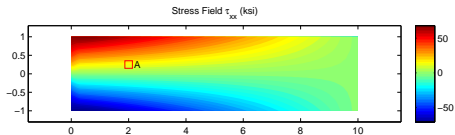
2. Principal stresses and directions in stress analysis

Stress block from point A



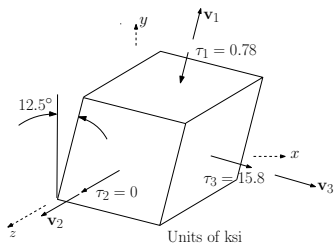
$$\boldsymbol{\tau} = \begin{bmatrix} \tau_{xx} & \tau_{xy} & \tau_{xz} \\ \tau_{xy} & \tau_{yy} & \tau_{yz} \\ \tau_{xz} & \tau_{yz} & \tau_{zz} \end{bmatrix}$$

$$\boldsymbol{\tau} = \begin{bmatrix} 15 & -3.5 & 0 \\ -3.5 & 0 & 0 \\ 0 & 0 & 0 \end{bmatrix}$$



2. Principal stresses and directions in stress analysis

MATLAB solution to eigen problem:



$$\tau_1 = -0.78, \mathbf{v}_1 = \begin{bmatrix} 0.2166 \\ 0.9763 \\ 0.0000 \end{bmatrix},$$

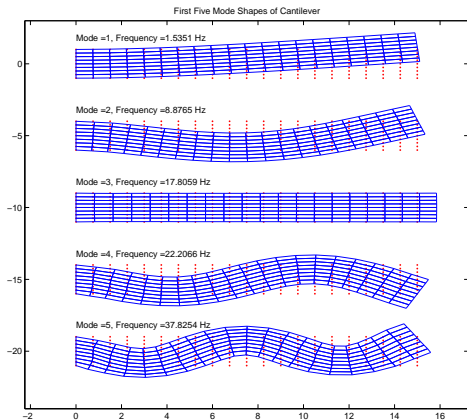
$$\tau_2 = 0.00, \mathbf{v}_2 = \begin{bmatrix} 0.0000 \\ 0.0000 \\ 1.0000 \end{bmatrix},$$

$$\tau_3 = 15.8, \mathbf{v}_3 = \begin{bmatrix} 0.9763 \\ -0.2166 \\ 0.0000 \end{bmatrix}$$

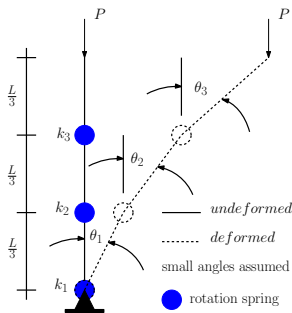
3. Fundamental frequencies and mode shapes in vibrations

Numerical Eigen problem solution

- 2D FEA of cantilever
- x & y dofs at 189 nodes
(2 x 189 = 378 dofs)
- \Rightarrow 378 eigenvalues & eigenvectors
- \Rightarrow 378 frequencies & mode shapes
- Eigenvectors are 378th dimensional vectors!
- $\bar{\mathbf{K}}\mathbf{v} = \lambda\mathbf{v}$, $\bar{\mathbf{K}} = 378 \times 378$ in this example!
- Finer Grid=More accurate



4. Critical loads & buckled shapes in buckling analysis



A deformed shape equilibrium analysis results in the following:

$$\begin{bmatrix} (k_1 + k_2) & -k_2 & 0 \\ -k_2 & (k_2 + k_3) & -k_3 \\ 0 & -k_3 & k_3 \end{bmatrix} \begin{bmatrix} \theta_1 \\ \theta_2 \\ \theta_3 \end{bmatrix} = \frac{PL}{3} \begin{bmatrix} \theta_1 \\ \theta_2 \\ \theta_3 \end{bmatrix}$$

$$\mathbf{K}\boldsymbol{\theta} = \lambda\boldsymbol{\theta}$$

4. Critical loads & buckled shapes in buckling analysis

For the case of

$L = 10$ inches

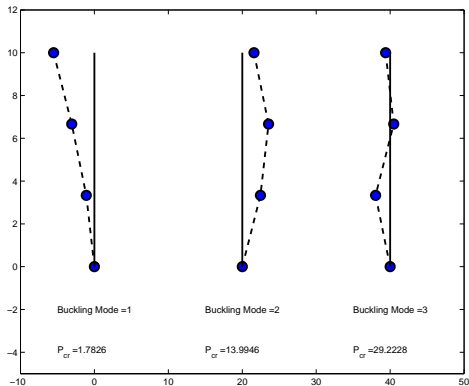
$k_1 = 30$ kip-in/rad

$k_2 = 30$ kip-in/rad

$k_3 = 30$ kip-in/rad

Eigenvalue = $\frac{P_{cr}L}{3}$

Eigenvector \Rightarrow shape



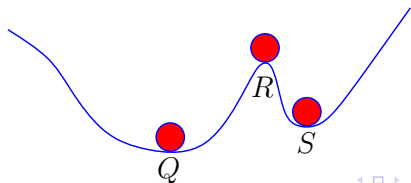
5. Applications in electrical engineering - feedback and control

Outline of conceptual feedback and control

- Model dynamic system such as airplane, car, rocket
- $\mathbf{M}\ddot{\phi} + \mathbf{C}\dot{\phi} + \mathbf{K}\phi = \mathbf{F}(t)$
- The mathematical model of the system has inherent eigenvalues and eigenvectors
- Eigenvalues describe resonant frequencies where the system will have its largest, often excessive, response.
- We can choose $\mathbf{F}(t)$ to reduce the system response at the resonant frequencies.

5. Applications in electrical engineering - feedback and control

- Perhaps let $\mathbf{F}(t) = \mathbf{A}\dot{\phi} + \mathbf{B}\phi$ and insert into dynamic system model
- The new system is $\mathbf{M}\ddot{\phi} + \bar{\mathbf{C}}\dot{\phi} + \bar{\mathbf{K}}\phi = \mathbf{0}$
- where $\bar{\mathbf{C}} = \mathbf{C} - \mathbf{A}$ = velocity dependent damping
- and $\bar{\mathbf{K}} = \mathbf{K} - \mathbf{B}$ = displacement dependent forcing
- We can adjust \mathbf{A} and \mathbf{B} so that the eigenvalues of the new 'barred' system are different from the original system
- By doing so we cause (control) the system to avoid excessive vibration or instability



6. Principal mass moment of inertia in 3D

3D kinetics of a rigid body

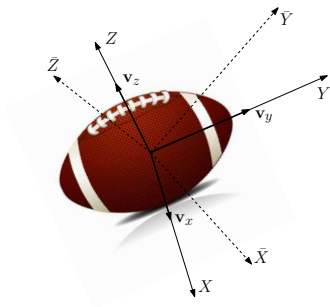
Inertia tensor (components dependent on $\bar{X}\bar{Y}\bar{Z}$ coordinate axes orientation)

$$I = \begin{bmatrix} I_{xx} & -I_{xy} & -I_{xz} \\ -I_{yx} & I_{yy} & -I_{yz} \\ -I_{zx} & -I_{zy} & I_{zz} \end{bmatrix}$$

It is possible to orient the axes such that

$$I = \begin{bmatrix} I_x & 0 & 0 \\ 0 & I_y & 0 \\ 0 & 0 & I_z \end{bmatrix}$$

6. Principal mass moment of inertia in 3D



In $\bar{X}\bar{Y}\bar{Z}$ coordinate system

$$I = \begin{bmatrix} I_{xx} & -I_{xy} & -I_{xz} \\ -I_{yx} & I_{yy} & -I_{yz} \\ -I_{zx} & -I_{zy} & I_{zz} \end{bmatrix}$$

I_x, I_y, I_z are eigenvalues

$\mathbf{v}_x, \mathbf{v}_y, \mathbf{v}_z$ are eigenvectors wrt $\bar{X}\bar{Y}\bar{Z}$

In XYZ coordinates

$$I = \begin{bmatrix} I_x & 0 & 0 \\ 0 & I_y & 0 \\ 0 & 0 & I_z \end{bmatrix}$$

Conclusion

A few comments:

- Many applications of eigenvalues and eigenvectors in engineering
- \mathbf{K} is not always symmetric
- eigenvalues are not always positive or real
- eigenvectors are orthogonal
- eigenvalues are invariant wrt to choice of coordinate axes

$$\mathbf{K}\theta = ?\theta$$