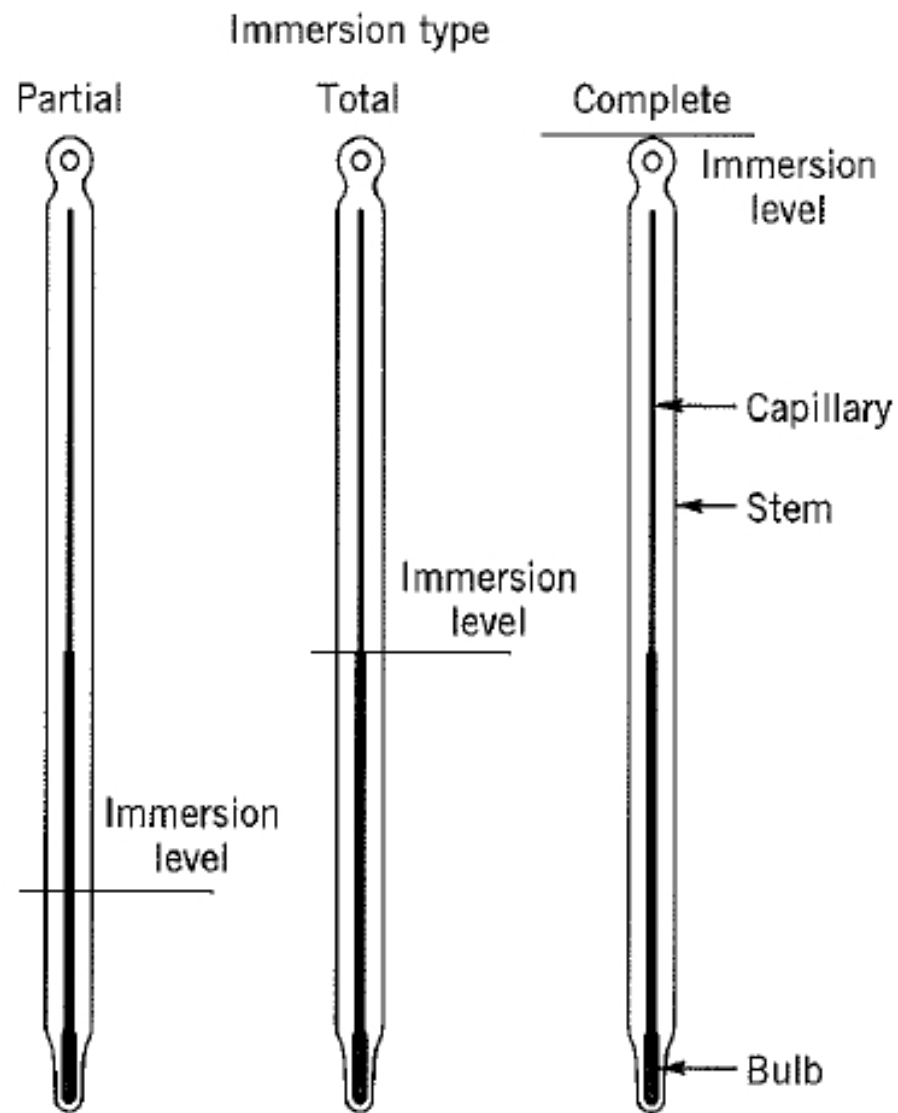
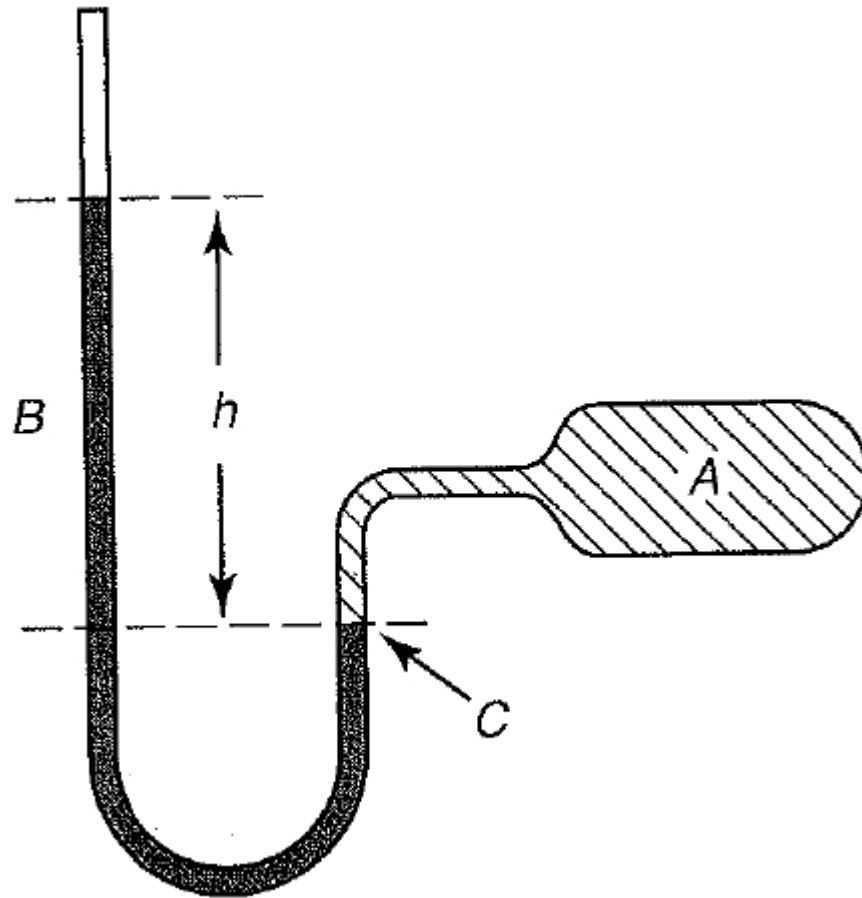


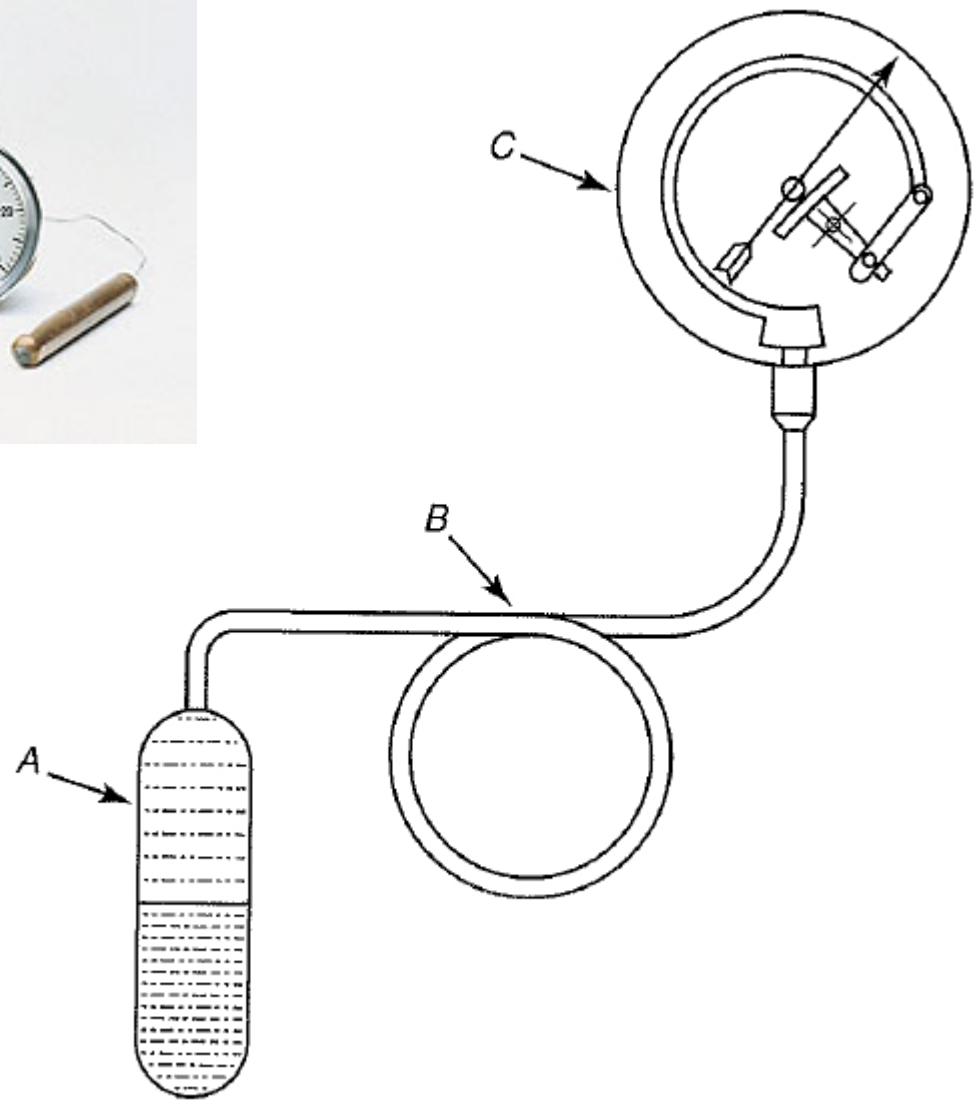
Temperature Measurement



Glass thermometers - 3 calibrations



Constant volume thermometer



Pressure thermometer

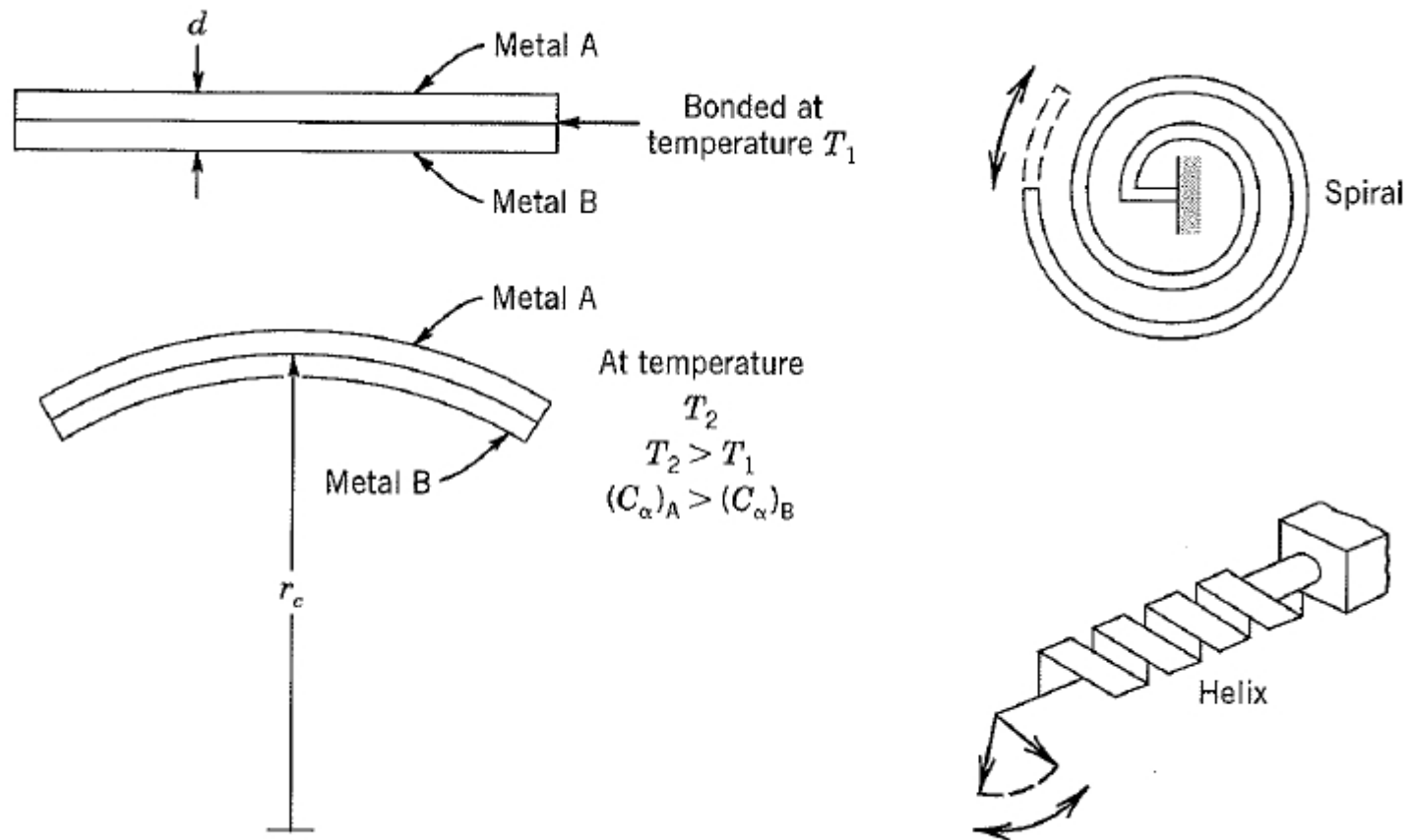


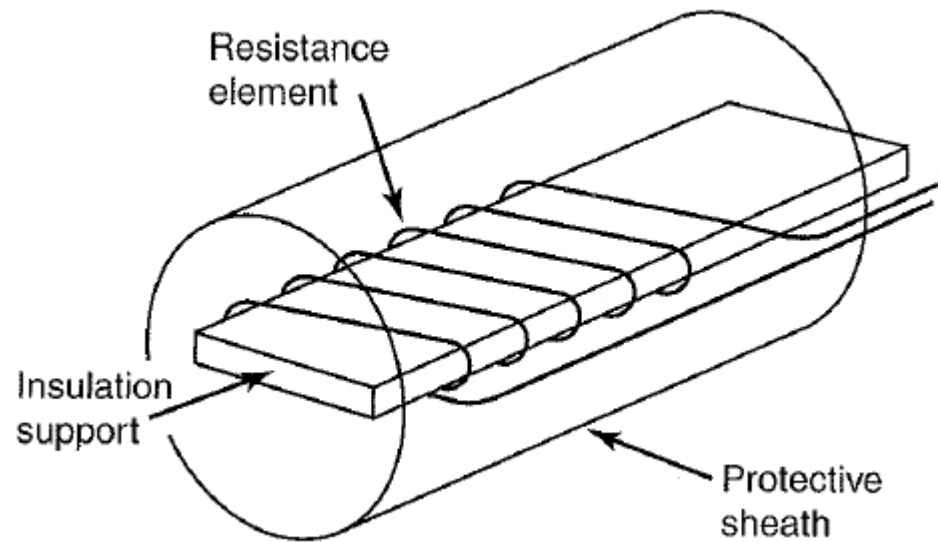
Figure 8.3 Expansion thermometry: bimetallic strip.

Invar $C = 1.7 \times 10^{-8} \text{ m/m degree C}$

Iron $C = 1.2 \times 10^{-5} \text{ m/m degree C}$



Resistive Temperature Detector - RTD



$$R = R_0[1 + \alpha(T - T_0) + \beta(T - T_0)^2 + \dots]$$

$$R = R_0[1 + \alpha(T - T_0)]$$

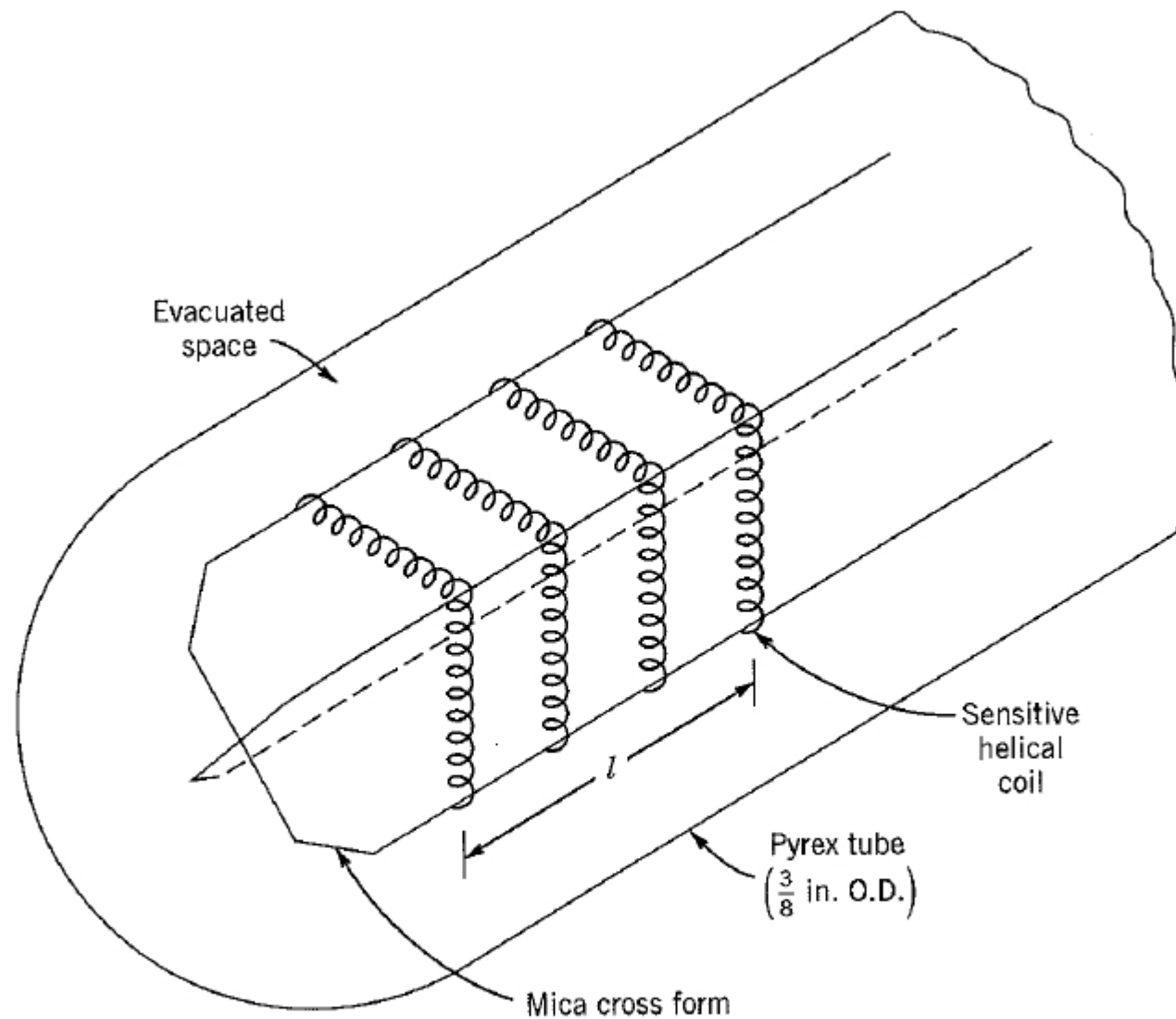
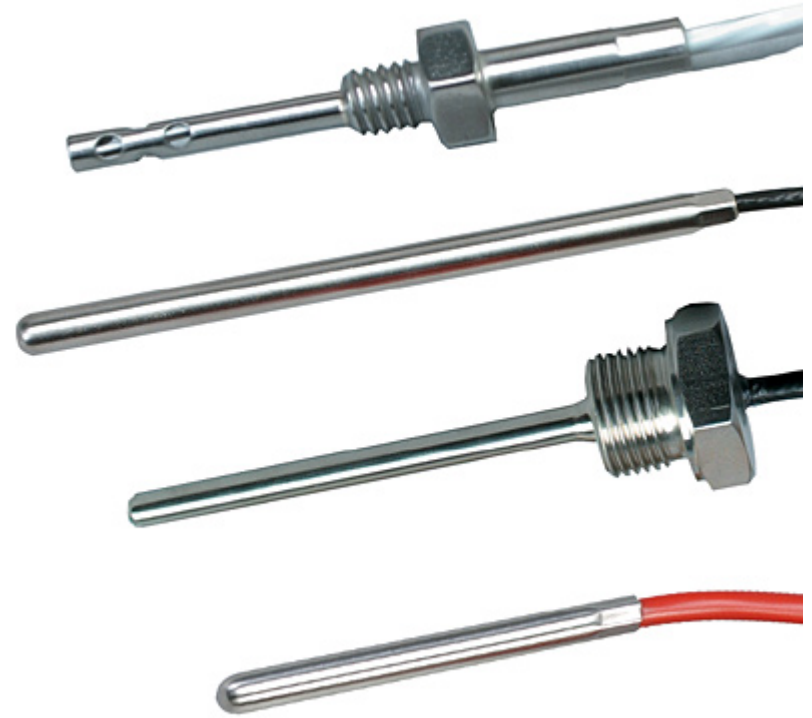
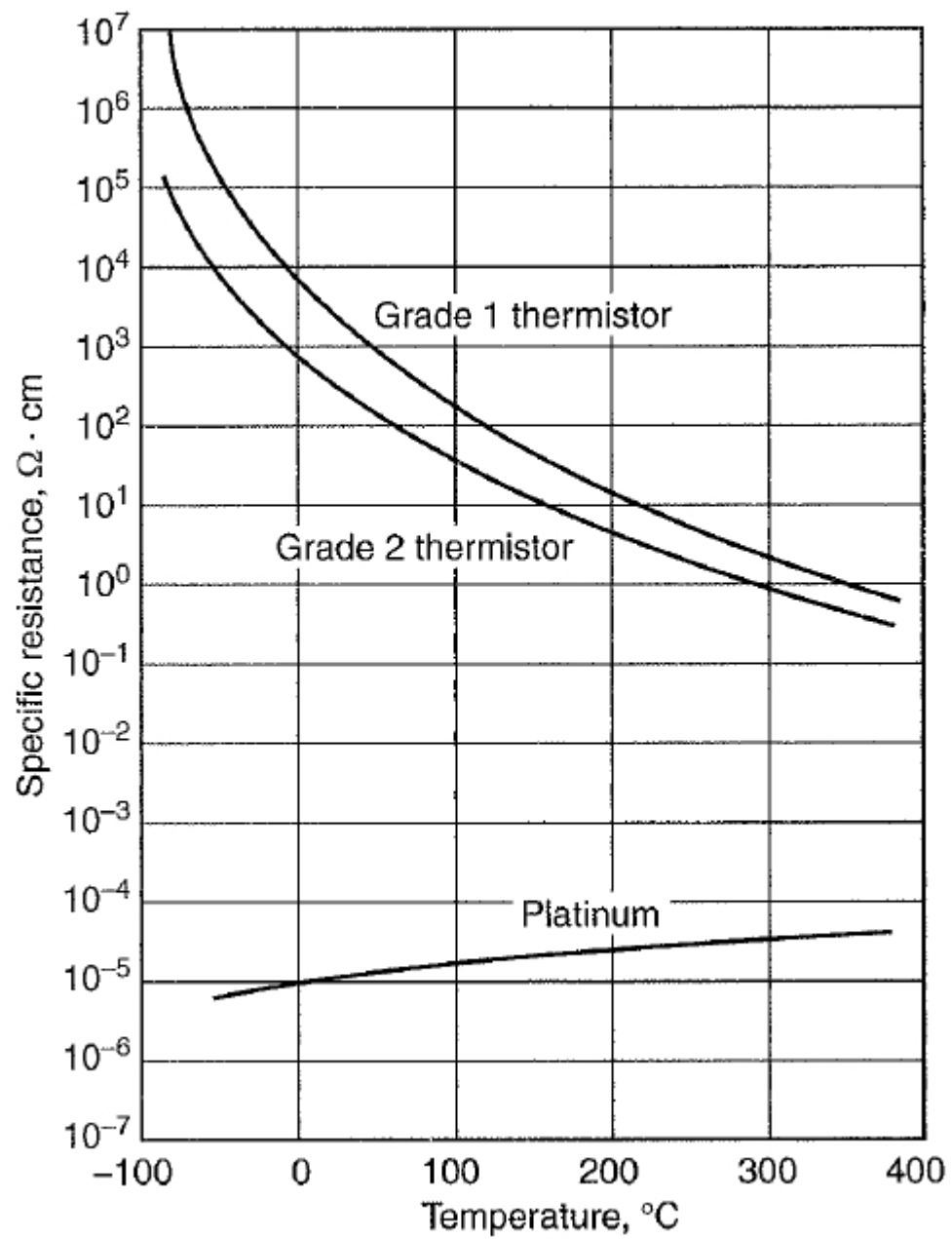


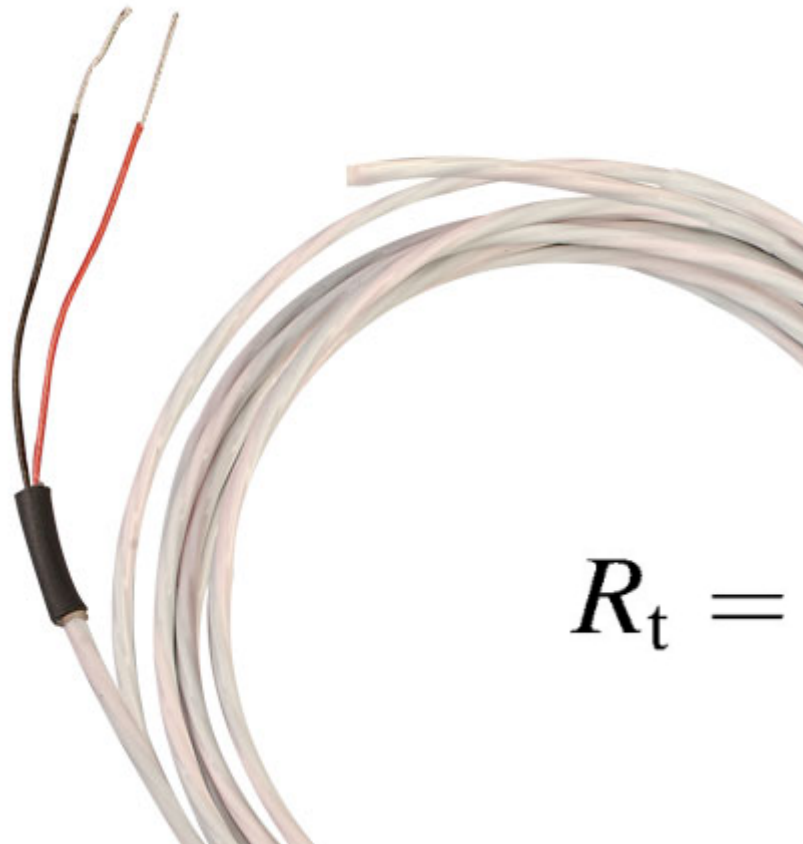
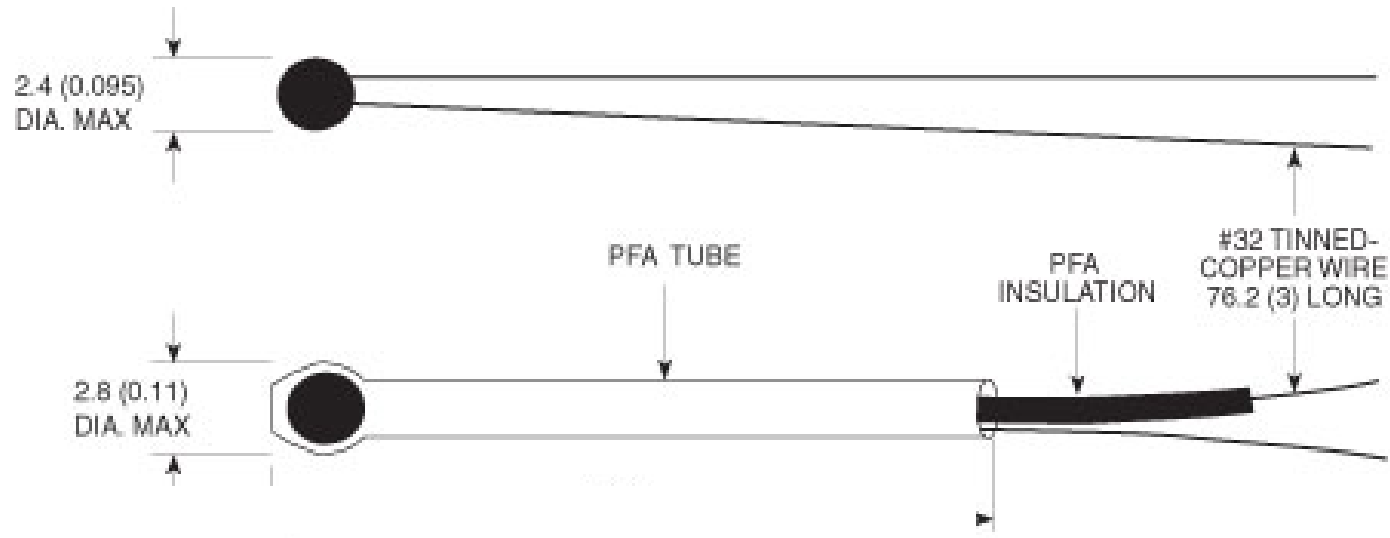
Figure 8.4 Construction of a platinum RTD. (From R. P. Benedict, *Fundamentals of Temperature, Pressure and Flow Measurements*, 3d ed., Wiley, New York, 1984.)



RTD sensors



Thermistor



$$R_t = R_0 e^{\beta(T_0 - T)/TT_0}$$

Sheathed thermistor probe

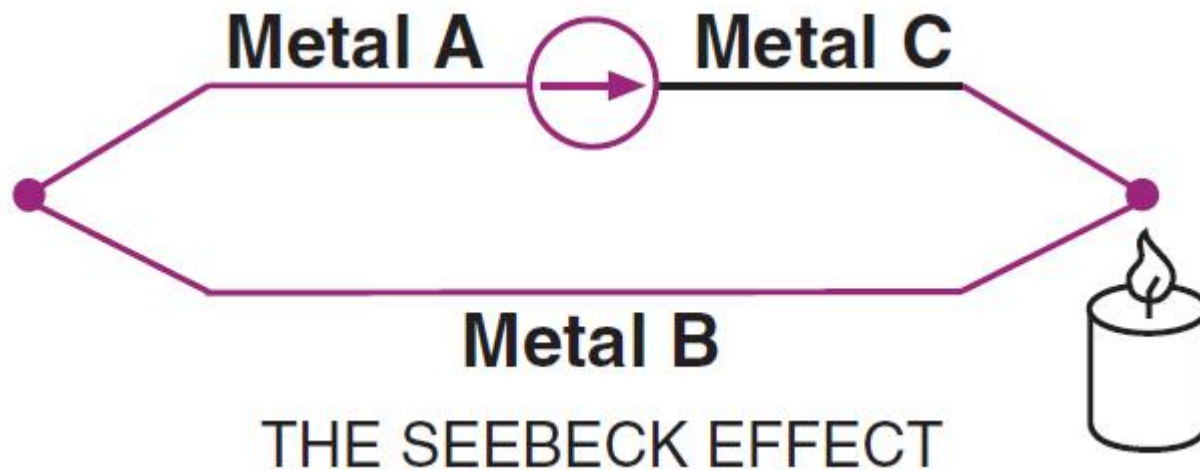


Thermistors

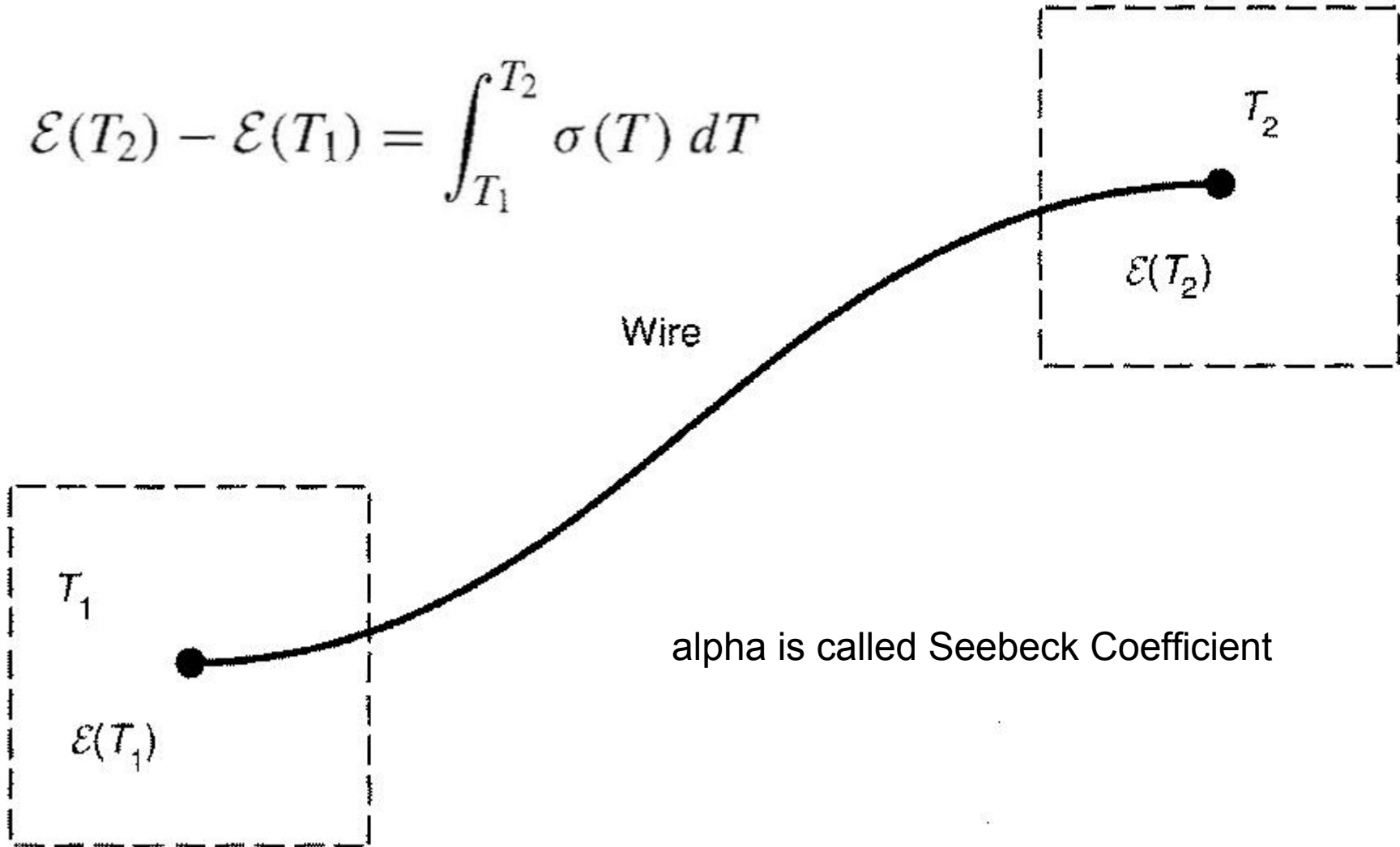


Thermocouple operation

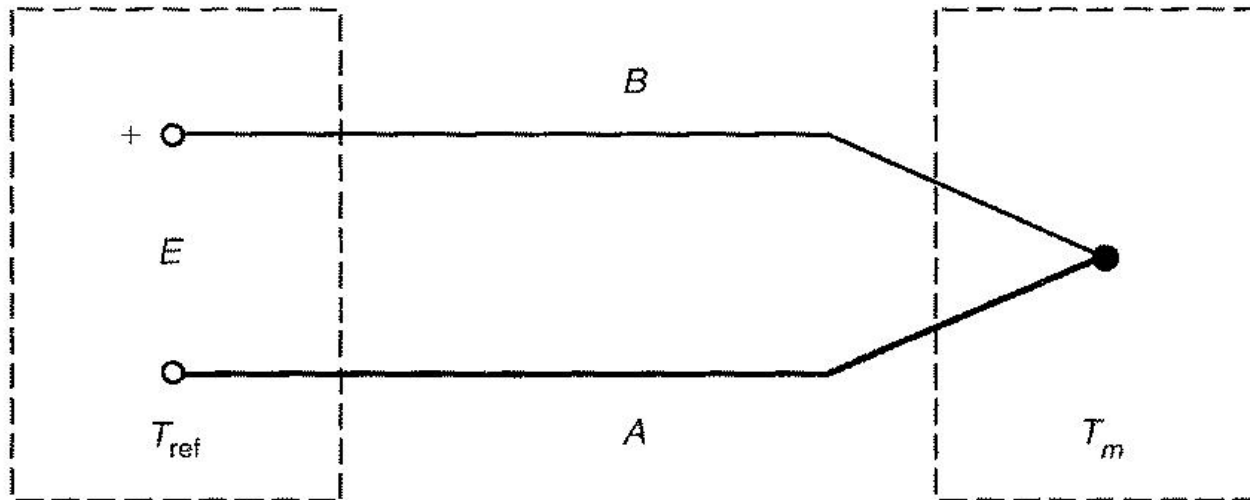
When two wires composed of dissimilar metals are joined at both ends and one of the ends is heated, there is a continuous current which flows in the *thermoelectric* circuit. Thomas Seebeck made this discovery in 1821.



$$\mathcal{E}(T_2) - \mathcal{E}(T_1) = \int_{T_1}^{T_2} \sigma(T) dT$$



alpha is called Seebeck Coefficient



$$\begin{aligned}
 E &= \int_{T_{\text{ref}}}^{T_m} \sigma_A dT + \int_{T_m}^{T_{\text{ref}}} \sigma_B dT \\
 &= [\mathcal{E}_A(T_m) - \mathcal{E}_A(T_{\text{ref}})] + [\mathcal{E}_B(T_{\text{ref}}) - \mathcal{E}_B(T_m)] \\
 &= [\mathcal{E}_A(T_m) - \mathcal{E}_B(T_m)] - [\mathcal{E}_A(T_{\text{ref}}) - \mathcal{E}_B(T_{\text{ref}})]
 \end{aligned}$$

Define: relative Seebeck emf ->
(of materials A and B)

$$\mathcal{E}_{AB}(T) \equiv \mathcal{E}_A(T) - \mathcal{E}_B(T)$$

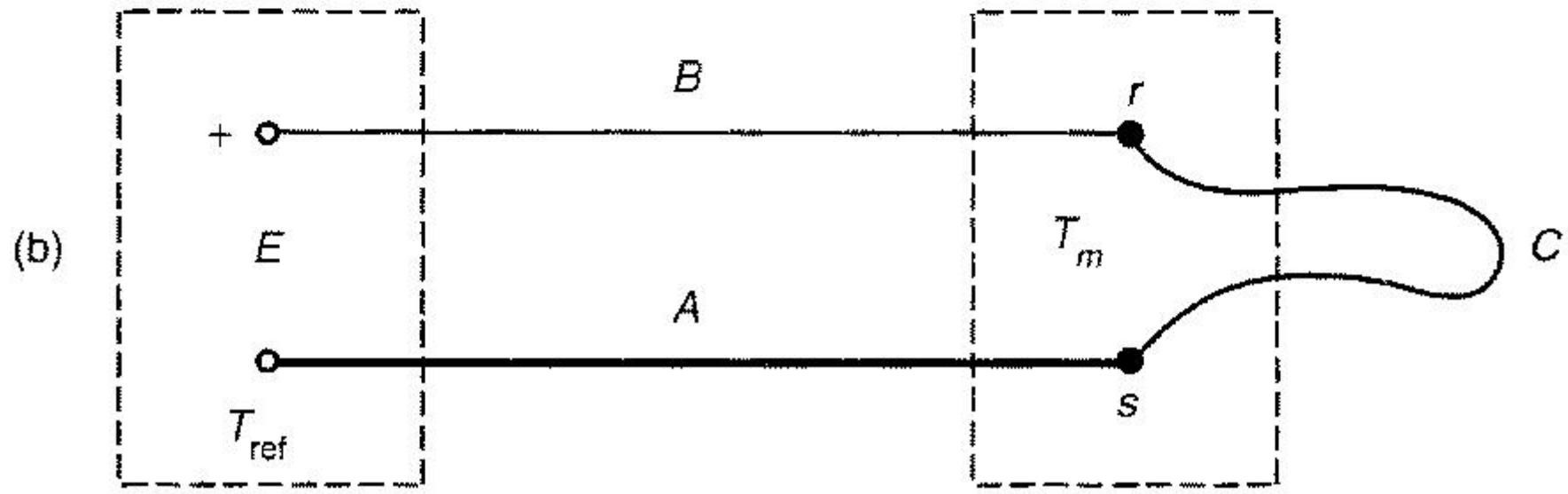
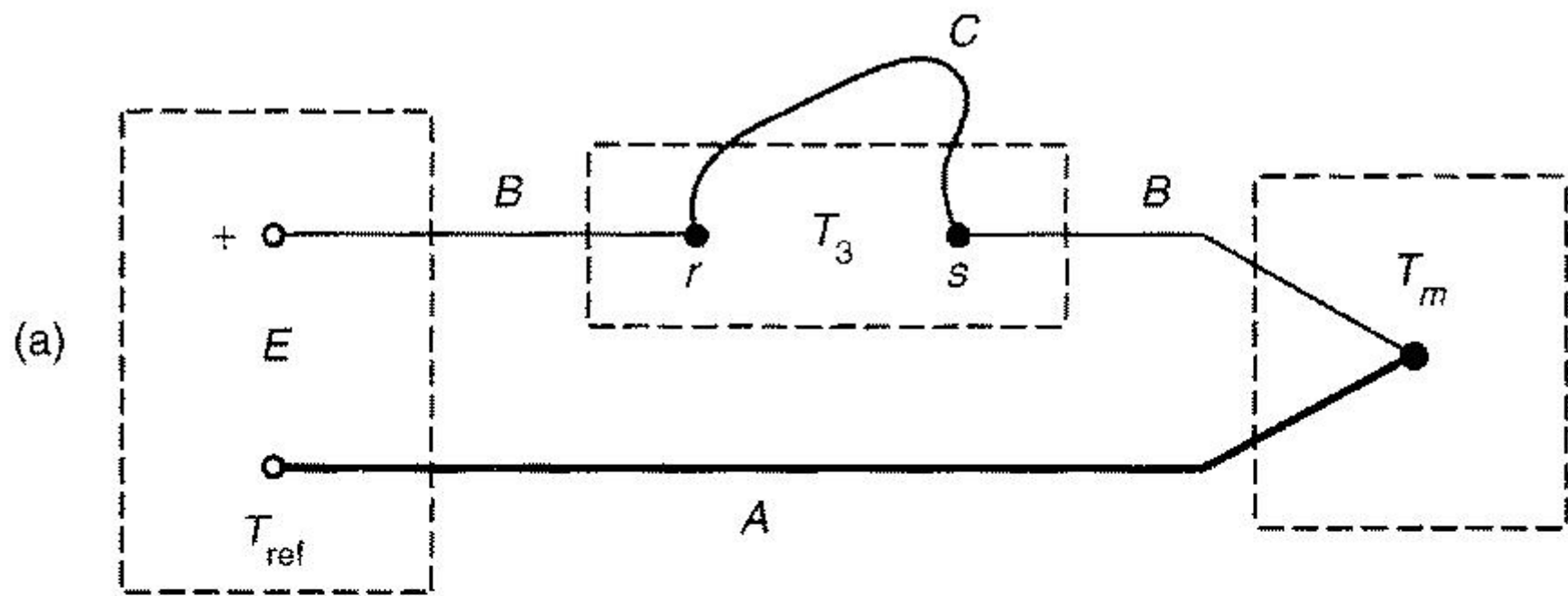
Then

$$E = \mathcal{E}_{AB}(T_m) - \mathcal{E}_{AB}(T_{\text{ref}})$$

| | | Type K | | | | |
|---------------------------------------|---------------------|--------|--------|--------|--------|--------|
| °C | | 0 | 5 | 10 | 15 | 20 |
| Thermocouple Voltage in millivolts | -200 | -5.891 | -5.813 | -5.730 | -5.642 | -5.550 |
| | -175 | -5.454 | -5.354 | -5.250 | -5.141 | -5.029 |
| | -150 | -4.913 | -4.793 | -4.669 | -4.542 | -4.411 |
| | -125 | -4.276 | -4.138 | -3.997 | -3.852 | -3.705 |
| | -100 | -3.554 | -3.400 | -3.243 | -3.083 | -2.920 |
| | -75 | -2.755 | -2.587 | -2.416 | -2.243 | -2.067 |
| | -50 | -1.889 | -1.709 | -1.527 | -1.343 | -1.156 |
| | -25 | -0.968 | -0.778 | -0.586 | -0.392 | -0.197 |
| | Reference = 0 deg C | 0 | 0.000 | 0.198 | 0.397 | 0.597 |
| | 25 | 1.000 | 1.203 | 1.407 | 1.612 | 1.817 |
| | 50 | 2.023 | 2.230 | 2.437 | 2.644 | 2.851 |
| | 75 | 3.059 | 3.267 | 3.474 | 3.682 | 3.889 |
| | 100 | 4.096 | 4.303 | 4.509 | 4.715 | 4.920 |
| | 125 | 5.124 | 5.328 | 5.532 | 5.735 | 5.937 |
| | 150 | 6.138 | 6.340 | 6.540 | 6.741 | 6.941 |
| | 175 | 7.140 | 7.340 | 7.540 | 7.739 | 7.939 |
| | 200 | 8.139 | 8.338 | 8.539 | 8.739 | 8.940 |
| | 225 | 9.141 | 9.343 | 9.545 | 9.747 | 9.950 |
| | 250 | 10.153 | 10.357 | 10.561 | 10.766 | 10.971 |
| | 275 | 11.176 | 11.382 | 11.588 | 11.795 | 12.002 |
| | 300 | 12.209 | 12.416 | 12.624 | 12.832 | 13.040 |
| | 325 | 13.248 | 13.457 | 13.665 | 13.875 | 14.084 |
| | 350 | 14.293 | 14.503 | 14.713 | 14.923 | 15.133 |
| | 375 | 15.343 | 15.554 | 15.764 | 15.975 | 16.186 |

Law of intermediate metals

Insertion of an intermediate metal into a thermocouple circuit will not affect the net emf -
provided that the two junctions introduced by the third metal are at identical temperatures





For gas, electric, and arc welding



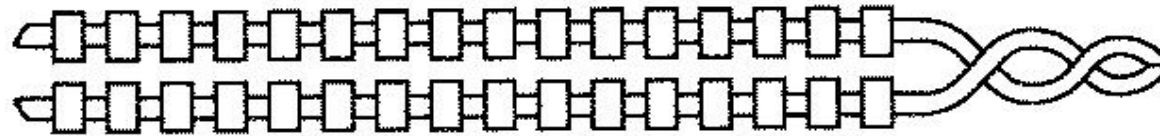
For resistance welding, large wires



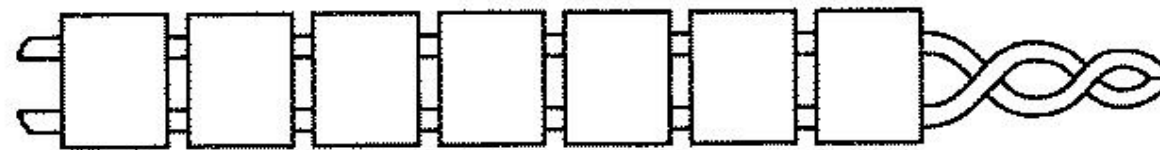
For forming noble-metal wires for electric arc welding



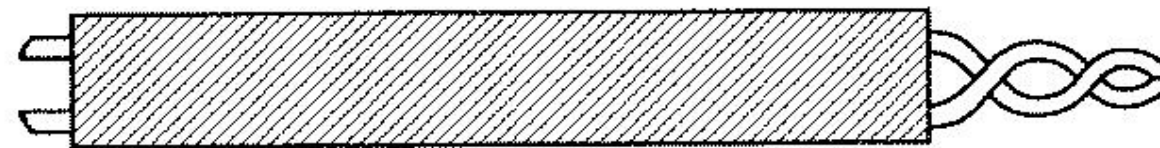
Bare element



Element with bead insulators



Element with double-bore insulators



Element with ceramic-tubing insulators

Termocouple voltages - in millivolts

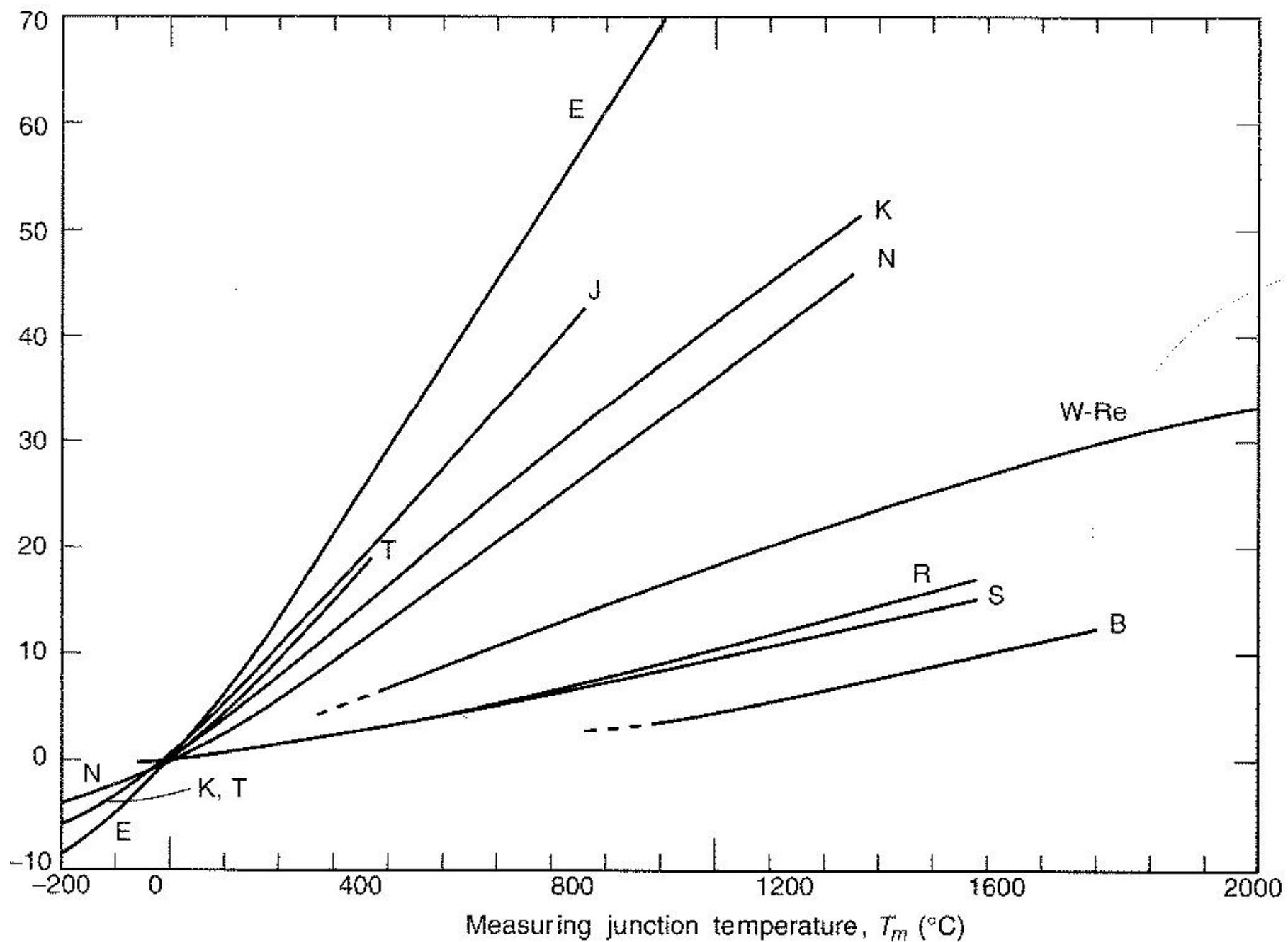
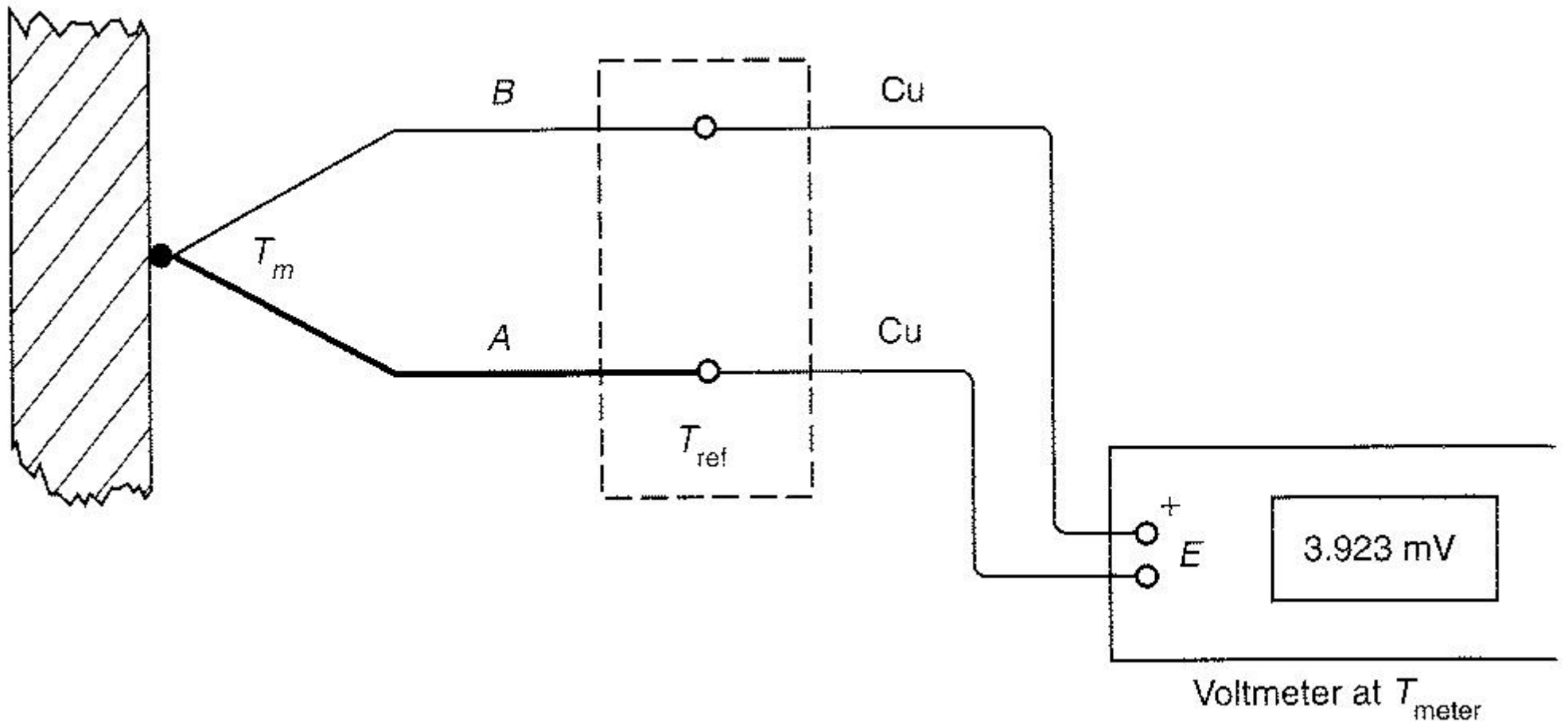
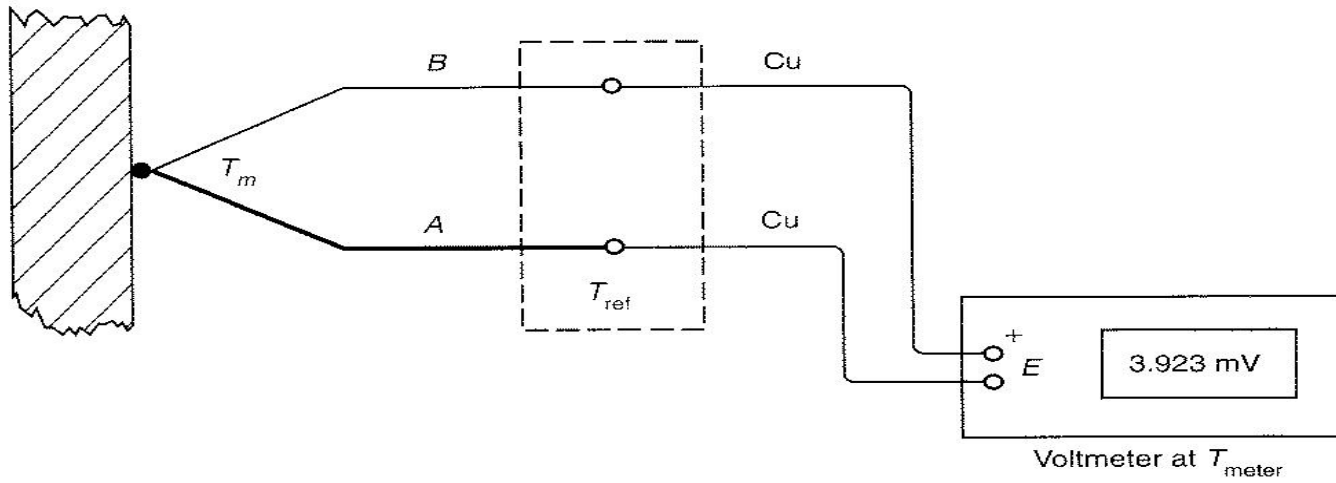


TABLE 16.4: Thermocouple Voltage E in Millivolts versus Temperature T_m for Reference Junctions at $T_{\text{ref}} = 0^\circ\text{C}$. Values Are Limited to the Recommended Range of Use [11]

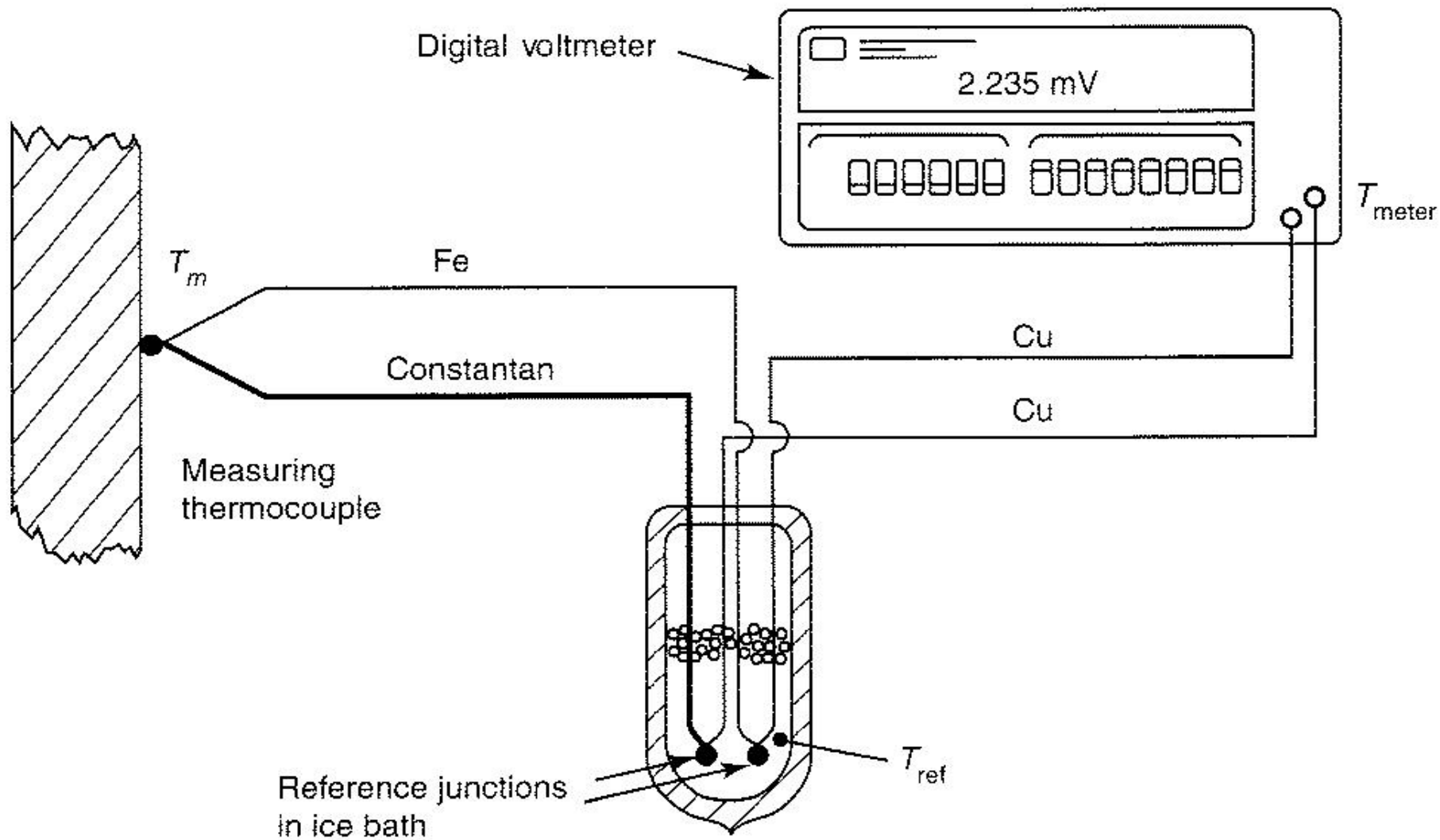
| Temperature $^\circ\text{C}$ ($^\circ\text{F}$) | Thermocouple Type | | | | |
|--|--------------------------------|-----------------------------|----------------------------|--------------------------------|-------------------------------|
| | Chromel vs. Constantan E | Iron vs. Constantan J | Chromel vs. Alumel K | Pt/10% Rh vs. Platinum S | Copper vs. Constantan T |
| -200 (-328) | -8.825 | | -5.891 | | -5.603 |
| -150 (-238) | -7.279 | | -4.913 | | -4.648 |
| -100 (-148) | -5.237 | | -3.554 | | -3.379 |
| -50 (-58) | -2.787 | | -1.889 | -0.236 | -1.819 |
| 0 (32) | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 50 (122) | 3.048 | 2.585 | 2.023 | 0.299 | 2.036 |
| 100 (212) | 6.319 | 5.269 | 4.096 | 0.646 | 4.279 |
| 150 (302) | 9.789 | 8.010 | 6.138 | 1.029 | 6.704 |
| 200 (392) | 13.421 | 10.779 | 8.139 | 1.441 | 9.288 |
| 300 (572) | 21.036 | 16.327 | 12.209 | 2.323 | 14.862 |
| 400 (752) | 28.946 | 21.848 | 16.397 | 3.259 | |
| 600 (1112) | 45.093 | 33.102 | 24.906 | 5.239 | |
| 800 (1472) | 61.017 | | 33.275 | 7.345 | |
| 1000 (1832) | | | 41.276 | 9.587 | |
| 1200 (2192) | | | 48.838 | 11.951 | |
| 1400 (2552) | | | | 14.373 | |





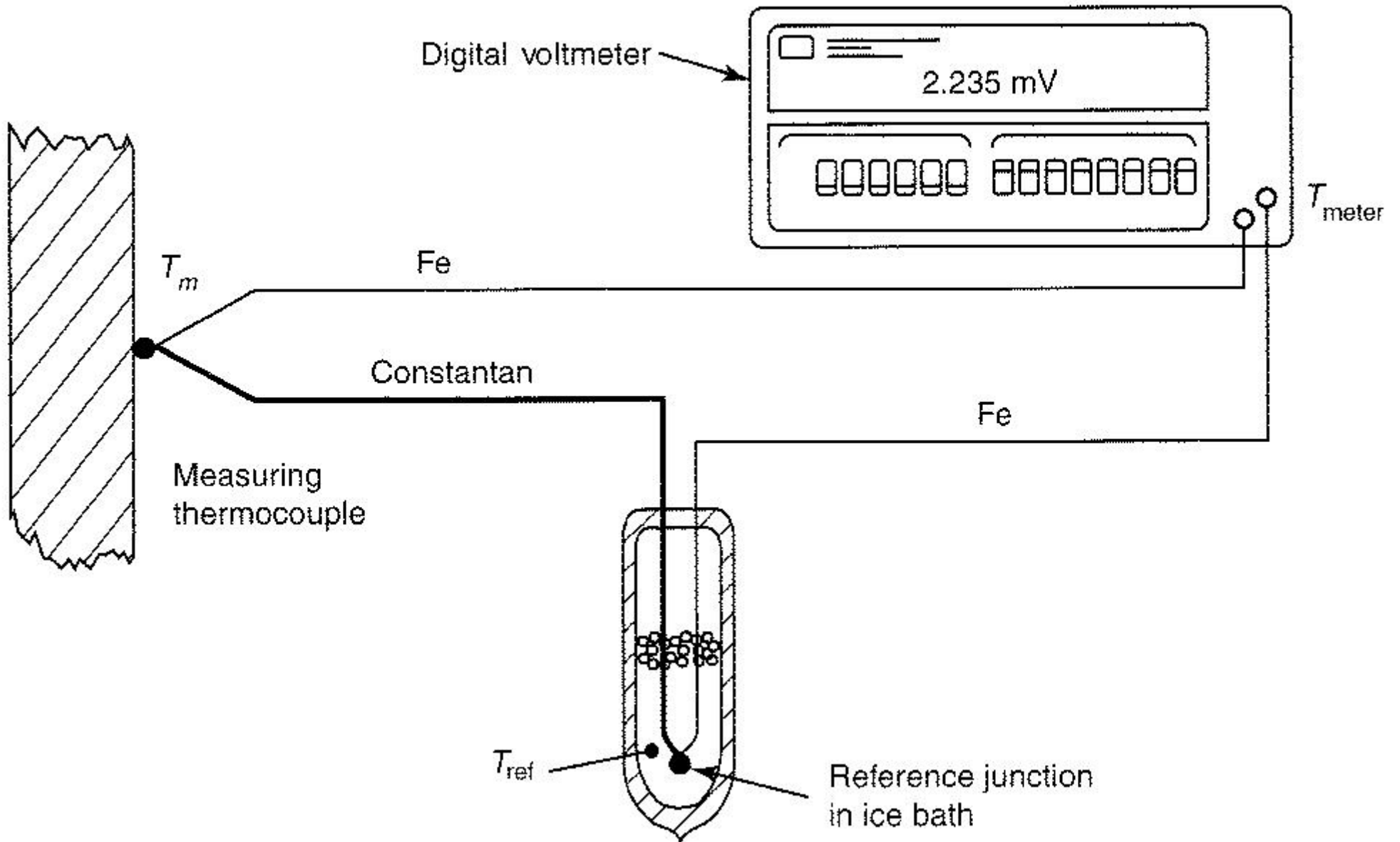
$$\begin{aligned}
 E &= [\mathcal{E}_{\text{Cu}}(T_{\text{ref}}) - \mathcal{E}_{\text{Cu}}(T_{\text{meter}})] + [\mathcal{E}_A(T_m) - \mathcal{E}_A(T_{\text{ref}})] \\
 &\quad + [\mathcal{E}_B(T_{\text{ref}}) - \mathcal{E}_B(T_m)] + [\mathcal{E}_{\text{Cu}}(T_{\text{meter}}) - \mathcal{E}_{\text{Cu}}(T_{\text{ref}})] \\
 &= \mathcal{E}_{AB}(T_m) - \mathcal{E}_{AB}(T_{\text{ref}})
 \end{aligned}$$

(a)

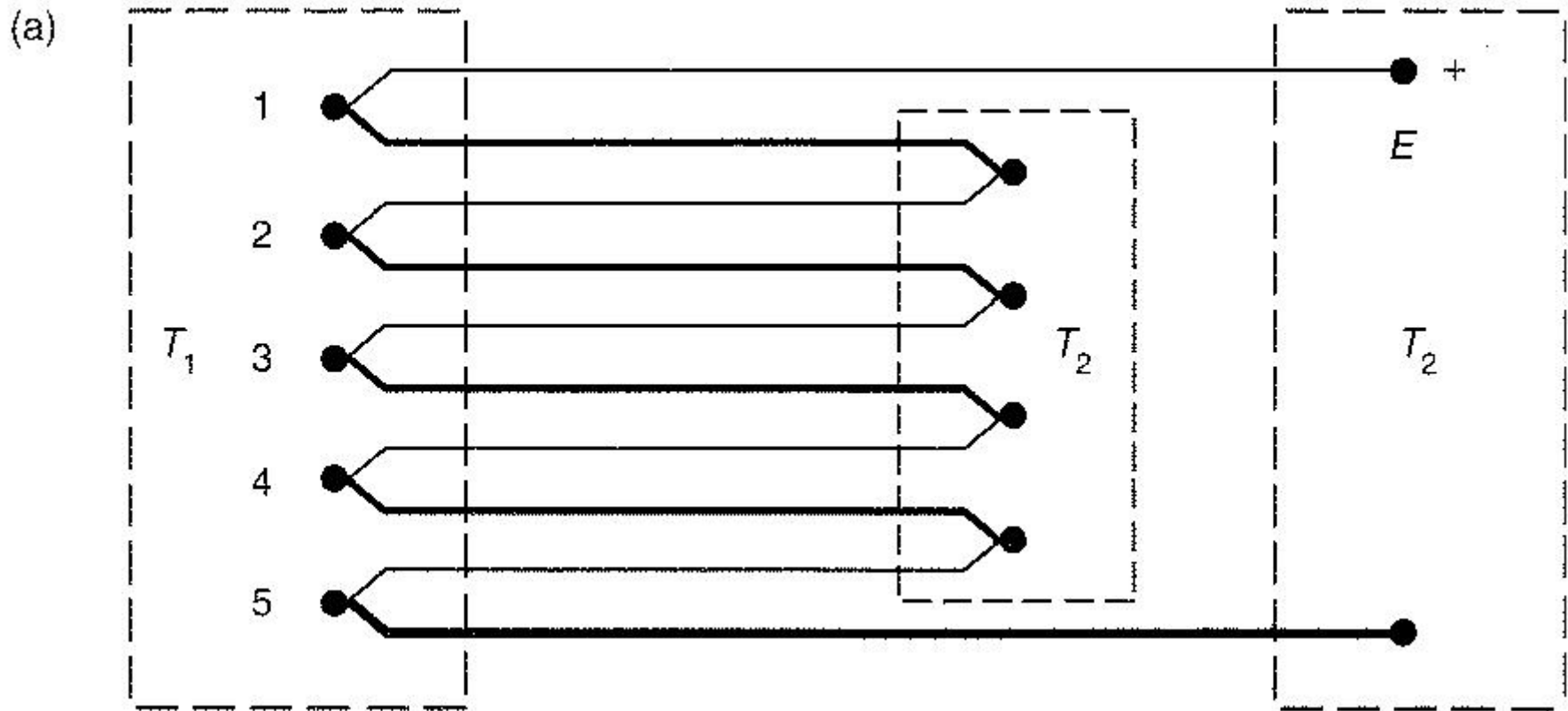


$$E = \mathcal{E}_{\text{FeCn}}(T_m) - \mathcal{E}_{\text{FeCn}}(0^\circ\text{C})$$

(b)



Thermocouples can be connected in series
Increases output voltage and averages



Thermocouples can be connected in parallel
Creates an average of T_1, T_2, T_3, T_4

(b)

