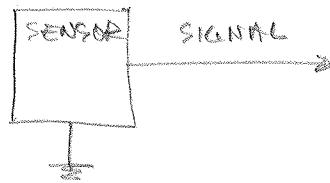


SUMMARY OF AMPLIFIERS, GROUNDING, SHIELDING

GROUNDING

SIGNALS MUST BE REFERENCED TO SOMETHING



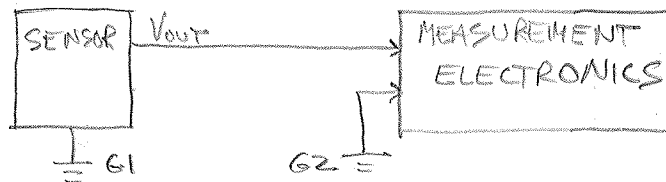
} IDEALIZED. CAN BE MISLEADING, APPEARS THAT WE ONLY NEED TO LOOK AT ONE SIGNAL LINE.

(FIG. 1)

NOTE: ALL SIGNAL SOURCES HAVE A MINIMUM OF TWO TERMINALS.

ALL RECEIVING CIRCUITS, I.E. AMPLIFIERS, HAVE TWO OR MORE TERMINALS.

ONE TERMINAL OFTEN IS STATED OR ASSUMED TO BE "GROUND"

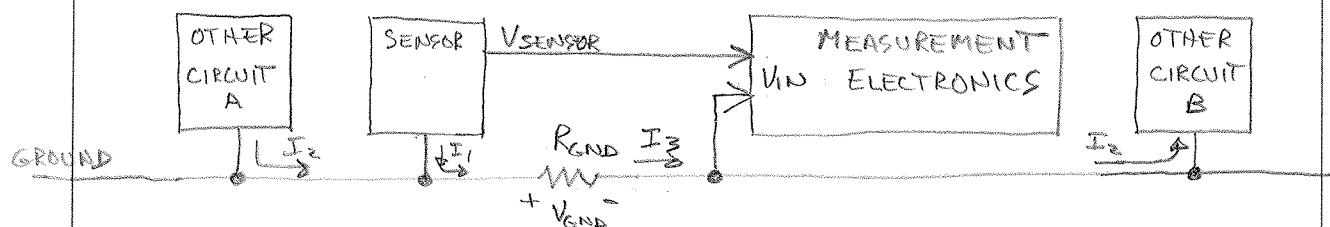


(FIG. 2)

CAUTION: AS SHOWN ABOVE, GROUND AT THE SENSOR IS ASSUMED TO BE AT THE SAME POTENTIAL AS GROUND AT THE MEASUREMENT ELECTRONICS. THIS EASILY CAN BE A FALSE ASSUMPTION.

NOTE WHAT CONNECTS GROUND 1 (G1) AND GROUND 2 (G2): AN UNDEFINED CONDUCTOR. THE MEASUREMENT ELECTRONICS WILL SENSE THE VOLTAGE BETWEEN ITS TWO INPUT TERMINALS.

POSSIBLE PROBLEM: NOISE INTRODUCED VIA COMMON SIGNAL PATH



(FIG. 3)

$$I_3 = I_1 + I_2 \quad \text{HOWEVER, ASSUME } I_1 \text{ SMALL. } \therefore I_3 = I_2$$

$$V_{IN} = V_{SENSOR} + V_{GND}$$

$$\therefore V_{IN} = V_{SENSOR} + \underbrace{I_2 R_{GND}}_{V_{NOISE}}$$

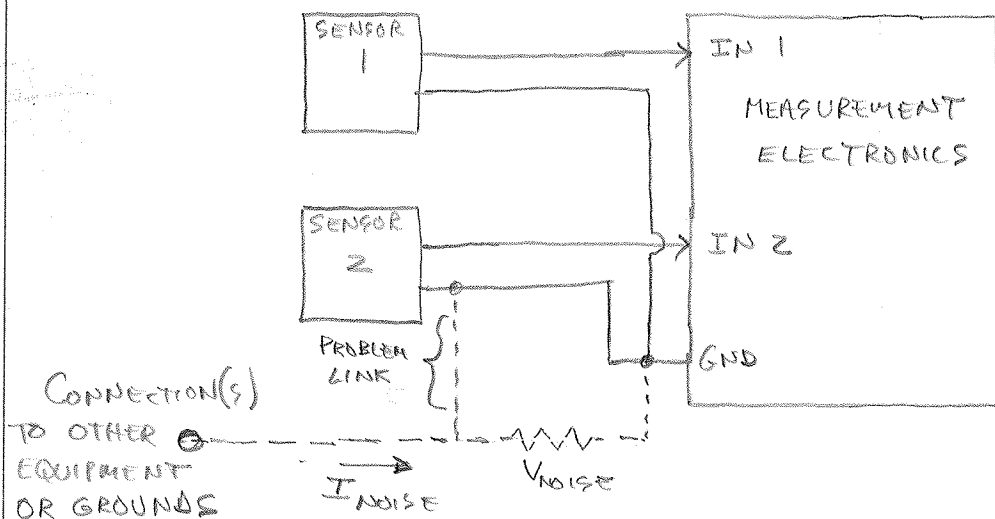
MORAL: GROUND CONNECTIONS MUST BE MADE CORRECTLY TO AVOID UNDESIRABLE ADDITION OF NOISE.

TWO TYPES OF AMPLIFIER INPUTS

SINGLE ENDED (UNBALANCED)

- INPUT SIGNALS ARE REFERENCED TO SOME INTERNAL SYSTEM GROUND
- IF THERE ARE MULTIPLE INPUTS ALL INPUTS ARE REFERENCED TO A COMMON GROUND

EXAMPLE



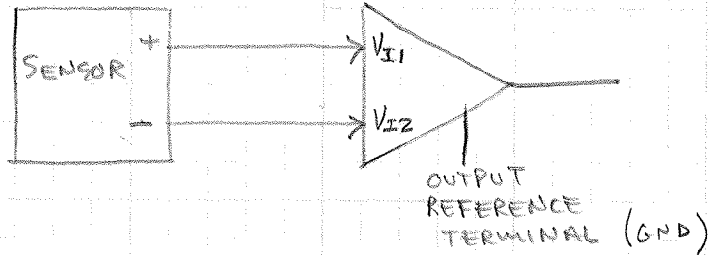
(FIG. 4)

- NOISE VOLTAGE WILL COUPLE INTO THE AMPLIFIER IF THE CIRCUIT IS GROUND AT MORE THAN ONE POINT

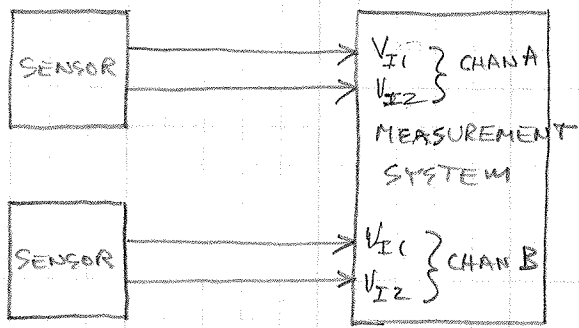
(AMPLIFIER INPUTS CONTINUED)

DIFFERENTIAL (BALANCED) AMPLIFIER INPUTS

- V_{IN} IS SENSED AS THE POTENTIAL BETWEEN THE TWO INPUTS, i.e. $(V_{I1} - V_{I2})$
 - THE IMPEDANCE SEEN LOOKING INTO EACH INPUT IS IDENTICAL
 - A VOLTAGE COMMON* TO BOTH INPUTS WILL CANCEL AND NOT AFFECT THE OUTPUT (* i.e. COMMON MODE VOLTAGE)
- } IDEAL BEHAVIOR



- IF DIFFERENTIAL INPUTS ARE USED FOR AN INSTRUMENTATION SYSTEM, THERE WILL BE TWICE AS MANY INPUT TERMINALS THAN A SINGLE ENDED SYSTEM

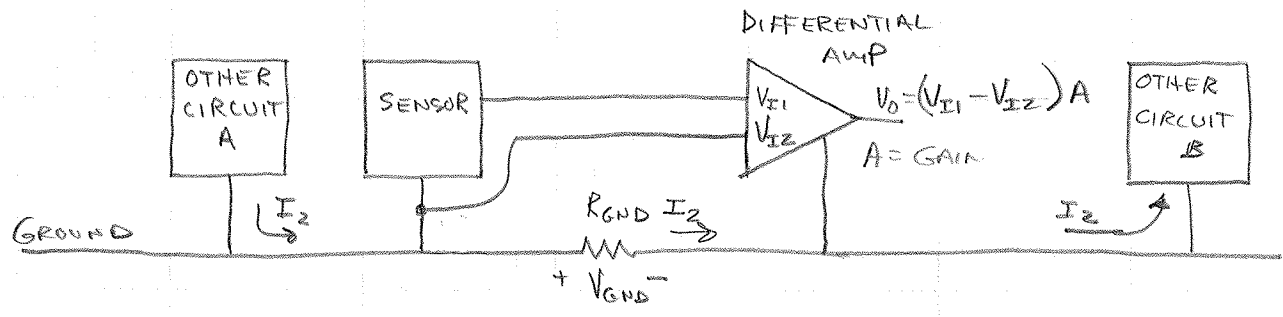


- PRACTICAL DIFFERENTIAL AMPLIFIERS HAVE A LIMITED COMMON MODE VOLTAGE RANGE
- REAL DIFFERENTIAL AMPLIFIERS DON'T PERFECTLY REJECT COMMON MODE VOLTAGE,
- COMMON MODE REJECTION RATIO (CMRR) IS A SPECIFICATION QUANTIFYING HOW WELL AN AMPLIFIER REJECTS COMMON MODE VOLTAGE. FOR EXAMPLE, IF CMRR = 60 DB, A COMMON MODE VOLTAGE WILL PRODUCE AN AMPLIFIER OUTPUT 0.001 OF WHAT IT WOULD

13-782 500 SHEETS, FILLER, 19 SQUARE
 42-881 50 SHEETS, CYCLAS, 8 SQUARE
 42-882 100 SHEETS, CYCLAS, 8 SQUARE
 42-883 200 SHEETS, CYCLAS, 8 SQUARE
 42-884 100 SHEETS, CYCLAS, 19 SQUARE
 42-885 100 RECYCLED WHITE, 8 SQUARE
 42-886 200 RECYCLED WHITE, 8 SQUARE
 Made in U.S.A.

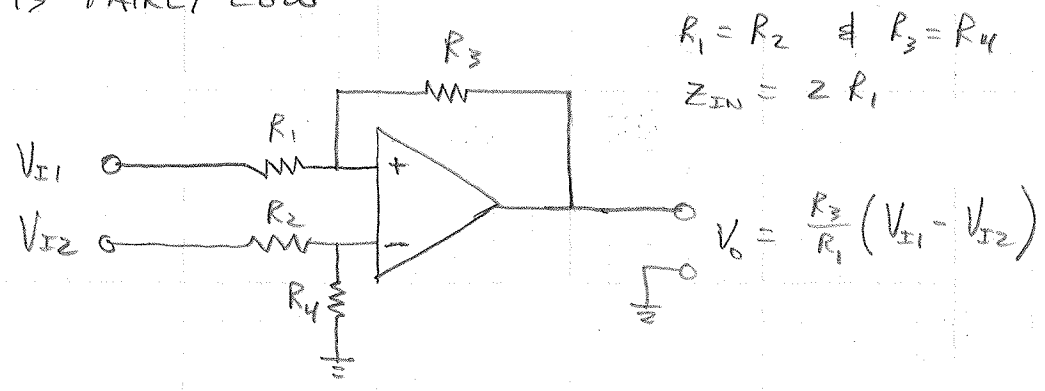


REDRAWING FIGURE 3 :



(FIG. 4)

- USING A DIFFERENTIAL AMPLIFIER, CONNECTIONS CAN BE MADE DIRECTLY BETWEEN AMP INPUT AND SENSOR OUTPUT. THE SENSOR OUTPUT CAN STILL BE REFERENCED (I.E. CONNECTED) TO A SYSTEM GROUND. BUT NOW V_{GND} CAUSED BY I_2 WILL BE SEEN AS A COMMON MODE VOLTAGE AND WILL BE REJECTED (TO THE EXTENT SPECIFIED BY CMRR)
- A DIFFERENTIAL AMPLIFIER WITH THESE CHARACTERISTICS, AMONG OTHERS, IS CALLED AN INSTRUMENTATION AMPLIFIER
 - GOOD COMMON MODE REJECTION
 - MATCHED IMPEDANCE FOR INPUTS V_{I1} & V_{I2} .
 - HIGH IMPEDANCE AT EACH INPUT
 - GAIN TYPICALLY SELECTABLE FROM 1 TO 1000
- A DIFFERENTIAL AMPLIFIER CAN BE CONSTRUCTED USING AN OP AMP, BUT THE INPUT IMPEDANCE IS FAIRLY LOW



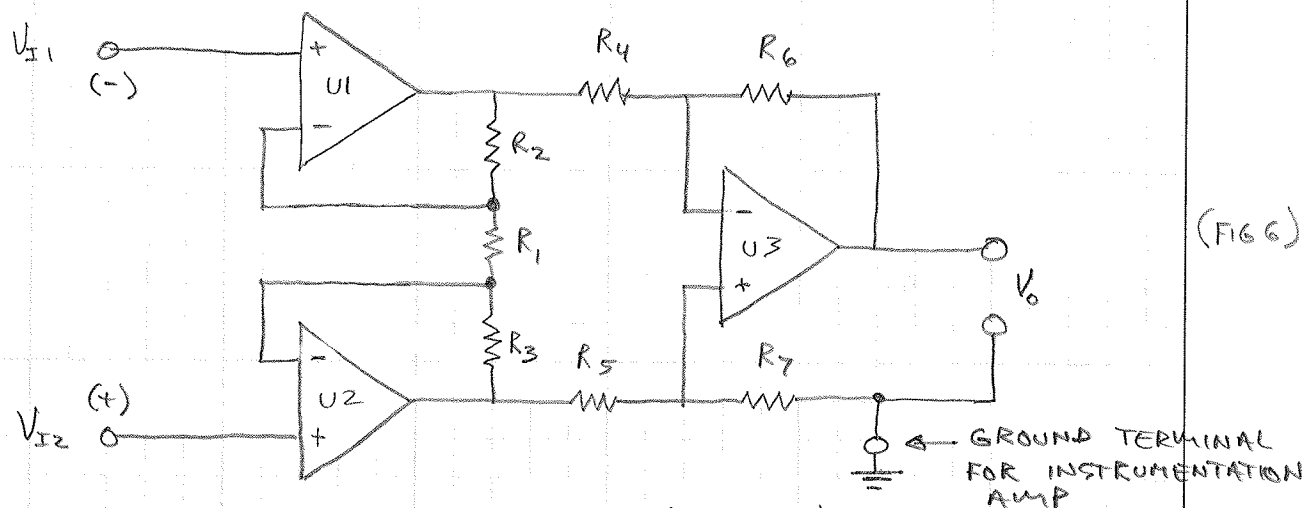
(FIG 5)

RESISTOR MATCHING MUST BE PRECISE TO ACHIEVE HIGH CMRR

13-782 500 SHEETS, FILLER, 5 SQUARE
 43-381 50 SHEETS, REAR, 5 SQUARE
 43-382 50 SHEETS, REAR, 5 SQUARE
 43-383 50 SHEETS, REAR, 5 SQUARE
 43-384 50 SHEETS, REAR, 5 SQUARE
 43-385 50 SHEETS, REAR, 5 SQUARE
 43-386 50 SHEETS, REAR, 5 SQUARE
 43-387 50 SHEETS, REAR, 5 SQUARE
 43-388 50 SHEETS, REAR, 5 SQUARE
 43-389 50 SHEETS, REAR, 5 SQUARE
 43-390 50 SHEETS, REAR, 5 SQUARE
 43-391 50 SHEETS, REAR, 5 SQUARE
 43-392 50 SHEETS, REAR, 5 SQUARE
 43-393 50 SHEETS, REAR, 5 SQUARE
 43-394 50 SHEETS, REAR, 5 SQUARE
 43-395 50 SHEETS, REAR, 5 SQUARE
 43-396 50 SHEETS, REAR, 5 SQUARE
 43-397 50 SHEETS, REAR, 5 SQUARE
 43-398 50 SHEETS, REAR, 5 SQUARE
 43-399 50 SHEETS, REAR, 5 SQUARE
 43-400 50 SHEETS, REAR, 5 SQUARE
 Made in U.S.A.



- A TRUE INSTRUMENTATION AMPLIFIER HAS A TOPOLOGY SIMILAR TO THIS:



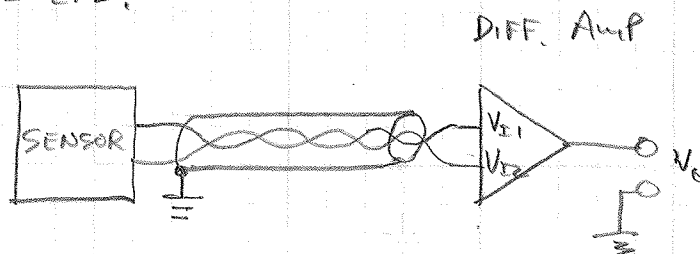
(FIG 6)

ASSUMPTIONS: $\begin{cases} R_2 = R_3 \\ R_4 = R_5 \\ R_6 = R_7 \end{cases}$ THEN: $V_O = G (V_{I1} - V_{I2})$
 $G = \left(1 + \frac{2R_2}{R_1}\right) \left(\frac{R_6}{R_4}\right)$

- AMPLIFIER INPUT IMPEDANCE IS DETERMINED BY THE INPUT CHARACTERISTICS OF U1 & U2.

REDUCING NOISE PICKUP IN WIRING

- 1- USE TWISTED PAIR WIRE BETWEEN SENSOR AND AMP
- 2- IF JUST TWISTED PAIR WIRE DOESN'T ADEQUATELY REJECT THE NOISE THEN USE TWISTED PAIR WITH A SHIELD AROUND IT. CONNECT THE SHIELD AT ONLY ONE END.



(FIG 7)

NOISE PICKED UP FROM THE ENVIRONMENT VIA ELECTRO-MAGNETIC COUPLING WILL TEND TO FLOW ON THE SHIELD TO GROUND AND THE TWISTED PAIR OF SIGNAL WIRES WON'T HAVE NOISE COUPLED TO THEM.

